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extends through aperture 53 in reflector 50 into the opaque chamber bounded by solid section 43, and then through a suitably provided bore in the lamp assembly housing where the stem is engaged by a rotatable drive shaft of motor 15 to permit rotation of the bulb about the stem axis. As is conventional, one of the effects produced by rotation of the bulb in this manner is the cooling of the bulb discharge envelope 23 in the microwave cavity.

Microwave energy entering the cavity defined by screen unit 20 via coupling slot 29 excites the fill in discharge envelope 23 resulting in light energy being emitted from the envelope. Reflective surface 51 prevents the light from entering the region of the microwave cavity bounded by solid section 43 of the cylindrical member 30. Instead, light impinging upon surface 51 is reflected out of the cavity through the interstices in mesh section 42 and end cap 40. Reflector 50, and in particular reflective surface 51, may be contoured as desired (e.g., concave, convex, etc.) to reflect light in preferential directions through the mesh. Clearly, substantially all of the light energy is prevented from passing into the region bounded by the solid section of the cylinder, thereby permitting the light to be most efficiently transmitted out through the interstices of the mesh material. Since the portions of the microwave cavity boundary wall through which light transmission is not desired are solid, the overall RF leakage through the screen unit is greatly reduced from that of an all mesh screen unit.

The lamp assembly described above may be utilized with an external reflector for focusing the light emitted through screen unit 20. Referring to FIG. 6, the assembly of FIGS. 1-5 is shown fitted with a substantially parabolic reflector 61 mounted on the lamp assembly by means of a bracket 62. Reflector 61 is positioned about mesh screen section 42 such that the bulb envelope 23 is disposed at or near the reflector focal point. The narrow end of reflector 61 is substantially co-planar with internal reflector 50 of the microwave cavity. The wide end of the reflector may be covered with a suitable glass cover.

As noted above, the cylindrical member of the screen unit is preferably fabricated by selectively etching the desired mesh pattern in a sheet of metal. It will be appreciated that the mesh pattern can easily take any shape consistent with the desired light transmission pattern for the lamp assembly. An example of another cylindrical member for a screen unit 70 formed in this manner is illustrated in FIG. 7. In this unit there are two solid metal sections, namely proximal cylindrical solid section 71, in which compliant attachment fingers 75 are formed, and a distal cylindrical solid section 73. Intermediate the two solid sections is a cylindrical mesh section 72. A proximate reflector 74 is secured at the juncture between proximal solid section 71 and mesh section 72 and has a domed convex reflective surface facing the optical transmission chamber in which the bulb discharge envelope 23 is located. A distal reflector 76 is secured at the juncture between distal solid section 73 and mesh section 72. Distal reflector 76 has a generally conical reflective surface converging toward the discharge envelope 23. Accordingly, all light emanating from the assembly is directed through the mesh section 72 of the screen unit closed by reflectors at its ends, and no mesh end cap is required. Such end cap (not illustrated) therefore may be solid and made from the same material as solid sections 71 and 73 of the cylinder.

An important advantage of the present invention is that it permits the entire assembly of FIG. 1 to be used interchangeably with screens of different configuration to produce a variety of illumination patterns. More specifically, and by way of example only, the screen unit in FIGS. 2-5 can be

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replaced with the unit of FIG. 7. The advantage of this is that the screen is extremely inexpensive to manufacture as compared to the other components of the assembly.

It will be appreciated, therefore, that the cylindrical member 30 can be etched or otherwise formed with any combination of mesh and solid sections from one sheet of metal. By appropriately locating one or more reflectors in the resulting microwave cavity, the optically transmissive chamber of the cavity can be isolated from the remainder of the cavity, thereby minimizing RF leakage while optimizing light transmission.

Although the screen unit for the preferred embodiments illustrated herein includes a substantially cylindrical member, it will be appreciated that the microwave cavity, in some instances, need not be cylindrical. In this regard, the same techniques described hereinabove may be utilized to provide screen units having rectangular, polygonal, oval, or other transverse cross-sections.

It will also be appreciated that the resulting screen unit of the present invention is very inexpensive to manufacture. Accordingly, if different optical configurations are required for a product line, the same overall lamp module assembly 10 may be utilized with a different screen unit in which the mesh and solid sections are oriented to yield the desired emitted light pattern.

The present invention also eliminates the requirement of fabricating a screen with an attached metal ring to secure the screen to the lamp assembly. The compliant fingers provided in the screen unit of the present invention, in combination with the hose clamp arrangement, obviates the need for the prior art permanent ring (an expensive step in screen fabrication) and allows for rapid, easy attachment of the screen unit to the lamp assembly.

The screen unit of the present invention allows for a multitude of solutions for moving and removing heat from the bulb and optics of the system. For example, by pressurizing the volume at the proximal end of the screen unit (i.e., defined by the reflector, the solid portion of the screen unit and the waveguide), one may introduce a flow of air to the bulb for cooling purposes. One may also derive a alternative ways of utilizing this enclosed volume as a plenum to deliver air to parts requiring cooling. Still further, the continuous portions of the screen may be treated to absorb and radiate efficiently, allowing for heat transfer from the optics internal to the cavity to the outside environment.

In order to enhance the optical and/or microwave characteristics of the lamp, it is possible to coat or plate the mesh and the solid portions of the screen unit. These same coatings may be difficult or cost prohibitive if applied to the waveguide.

From the foregoing description it will be appreciated that the invention makes available a novel screen unit for electrodeless lamps wherein mesh and solid sections may be defined in a single member used to form the body of a microwave cavity, and wherein a reflector can be disposed at the juncture between the solid and mesh sections to optically isolate those sections to achieve improved light transmission while reducing microwave energy leakage from the cavity.

Having described preferred embodiments of a new and improved microwave containment screen for electrodeless discharge lamps, it is believed that other modifications, variations and changes will be suggested to persons skilled in the art in view of the teachings set forth herein. Accordingly, it is to be understood that all such variations, modifications and changes are believed to fall within the scope of the present invention as defined by the appended claims.

What is claimed is:

1. A microwave powered lamp comprising:

a source of microwave energy;

a microwave cavity having a one-piece peripheral boundary wall including a solid wall section substantially impervious to light and to said microwave energy, and a mesh wall section transmissive to light and not transmissive to said microwave energy;

an electrically non-conductive light reflector mounted within said cavity to subdivide said cavity into first and second chambers, said first chamber including said solid section of said peripheral boundary wall, said second chamber including at least part of said mesh section of said peripheral boundary wall, wherein said reflector optically isolates said second chamber and blocks light transmission between said chambers;

a discharge envelope containing material therein excitable by said microwave energy to emit light therefrom, said discharge envelope being maintained in said second chamber such that said light emitted from said envelope is transmitted through said mesh section both directly from said envelope and as reflected light from said reflector; and

coupling means directing said microwave energy from said source into said cavity to excite said material in said discharge envelope.

2. The lamp of claim 1 further comprising a drive motor for rotating said discharge envelope, wherein said discharge envelope is supported on a stem extending through said reflector, into and through said first chamber, and into rotatable engagement with said motor.

3. The lamp of claim 1 wherein said coupling means comprises a waveguide unit and a coupling slot disposed in a housing, said housing having a flange projecting outward from the housing and circumscribing said coupling slot;

wherein said microwave cavity is secured to said housing at said flange by plural compliant circumferentially spaced fingers projecting from said solid section and disposed about said flange, and a hose clamp compressing said fingers against said flange.

4. The lamp of claim 1 wherein said peripheral boundary wall is a one-piece sheet of metal through which said mesh section is defined over a prescribed area.

5. The lamp of claim 4 wherein said mesh section comprises multiple interstitial openings in said sheet.

6. The lamp of claim 5 wherein said solid and mesh sections comprise adjacent cylindrical sections, wherein said coupling means communicates directly with said first chamber of said cavity to direct said microwave energy into said first chamber.

7. The lamp of claim 6 wherein said mesh section is bounded by a narrow solid metal border, said border comprising a continuance of the solid section, and wherein said sheet is disposed about an axis to provide said peripheral boundary wall as a cylinder with said border along opposite edges of said sheet in overlapping and joined relation.

8. The lamp of claim 1, further comprising an external reflector positioned about said mesh wall section, for focusing said light transmitted through said mesh wall section.

9. A microwave powered lamp comprising:

a source of microwave energy;

a microwave cavity having a boundary wall including a single metal sheet having a solid optically non-

transmissive wall section and a mesh wall section defined therein;

coupling means for delivering said microwave energy to said cavity;

a discharge envelope mounted in said cavity and containing fill material therein responsive to excitation by said microwave energy for emitting light from said envelope; and

an electrically non-conductive reflector mounted in said cavity for defining an optically isolated light-transmitting chamber in said cavity wherein said reflector is positioned to reflect said light from said envelope into said chamber and out through said mesh wall section.

10. The lamp of claim 9 wherein said sheet has multiple compliant fingers defined in spaced relation along one edge thereof for securing said cavity to said coupling means.

11. The lamp of claim 9 wherein said mesh and solid wall sections meet at a juncture, and wherein said reflector is secured at said juncture to define said light-transmitting chamber between said mesh section and said reflector, leaving a remainder of said cavity bounded by the optically non-transmissive solid wall section and said reflector.

12. A method for constructing a microwave powered electrodeless lamp of the type having a discharge envelope disposed in a microwave cavity and containing fill material therein responsive to microwave energy for emitting light therefrom, said method comprising the steps of:

(a) forming a mesh pattern through part of a thin metal sheet to define adjacent mesh and solid sections in said sheet with a juncture between said sections;

(b) securing opposite edges of said sheet to one another to form a peripheral enclosure for said cavity;

(c) securing an electrically non-conductive light reflector in said cavity and proximate to an optical transmission chamber bounded at least in part by said reflector and said mesh section; and

(d) disposing said discharge envelope in said optical transmission chamber.

13. The method of claim 12 further comprising the steps of:

(e) securing said cavity to a waveguide assembly of said lamp by forming multiple compliant fingers along one edge of said sheet as part of step (a);

(f) disposing the compliant fingers about a continuous flange on said waveguide assembly; and

(g) radially constricting said fingers about said flange with a clamp.

14. The method of claim 12 further comprising the step of:

(e) securing said cavity to a waveguide assembly of said lamp.

15. The method of claim 14 further comprising the steps of:

(f) removing from said waveguide assembly the cavity secured thereto in step (e); and

(g) securing a second cavity to said waveguide assembly.

16. The method of claim 12 wherein step (a) includes etching said mesh pattern through said sheet.

17. A method for constructing a microwave powered electrodeless lamp of the type having a discharge envelope disposed in a microwave cavity of a lamp assembly and containing fill material therein responsive to microwave energy for emitting light therefrom, said method comprising the steps of:

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- (a) forming a mesh pattern through part of a one-piece metal sheet to define adjacent mesh and solid sections in said sheet with a juncture between said sections;
- (b) forming a peripheral screen unit with said sheet;
- (c) securing said screen unit to the lamp assembly to form an enclosure; and
- (d) disposing the discharge envelope in said enclosure.

18. A microwave powered lamp comprising:

a source of microwave energy;

a microwave cavity having a one-piece sheet boundary wall including a solid wall section substantially impervious to light and to said microwave energy, and a mesh wall section transmissive to light and not transmissive to said microwave energy;

a discharge envelope containing material therein excitable by said microwave energy to emit light therefrom, said discharge envelope being maintained in said cavity such that said light emitted from said envelope is transmitted through said mesh section;

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coupling means directing said microwave energy from said source into said cavity to excite said material in said discharge envelope; and wherein said mesh section comprises multiple interstitial openings in said sheet.

19. A microwave cavity for an electrodeless lamp, said cavity comprising:

a one-piece peripheral boundary wall including a solid wall section substantially impervious to light and to microwave energy, and a mesh wall section transmissive to light and not transmissive to said microwave energy.

20. A method of constructing a microwave cavity, comprising the steps of:

- (a) forming a mesh pattern through part of a thin metal sheet to define adjacent mesh and solid sections in said sheet with a juncture between said sections; and
- (b) securing opposite edges of said sheet to one another to form a peripheral enclosure defining said cavity.

* * * * *



US005773918A

United States Patent [19]

Dolan et al.

[11] **Patent Number:** 5,773,918[45] **Date of Patent:** *Jun. 30, 1998[54] **LAMP WITH LIGHT REFLECTION BACK INTO BULB**[75] **Inventors:** James T. Dolan, Frederick; Michael G. Ury, Bethesda, both of Md.[73] **Assignee:** Fusion Lighting, Inc., Rockville, Md.[*] **Notice:** The term of this patent shall not extend beyond the expiration date of Pat. No. 5,404,076.[21] **Appl. No.:** 488,279[22] **Filed:** Jun. 7, 1995**Related U.S. Application Data**

[62] Division of Ser. No. 149,818, Nov. 10, 1993, which is a continuation of Ser. No. 60,553, May 13, 1993, abandoned, which is a continuation-in-part of Ser. No. 867,551, Apr. 13, 1992, abandoned, Ser. No. 875,769, Apr. 29, 1992, abandoned, and Ser. No. 882,409, May 13, 1992, abandoned, which is a continuation-in-part of Ser. No. 779,718, Oct. 23, 1991, abandoned, which is a continuation-in-part of Ser. No. 604,487, Oct. 25, 1990, abandoned.

[51] **Int. Cl.⁶** H01J 17/20; H01J 61/12; H01J 61/18[52] **U.S. Cl.** 313/113; 313/572; 313/637; 313/638; 313/643; 315/248[58] **Field of Search** 313/110, 112, 313/113, 484-93, 567, 568, 572, 573, 634-37; 315/248, 267-68, 344; 362/345[56] **References Cited****U.S. PATENT DOCUMENTS**

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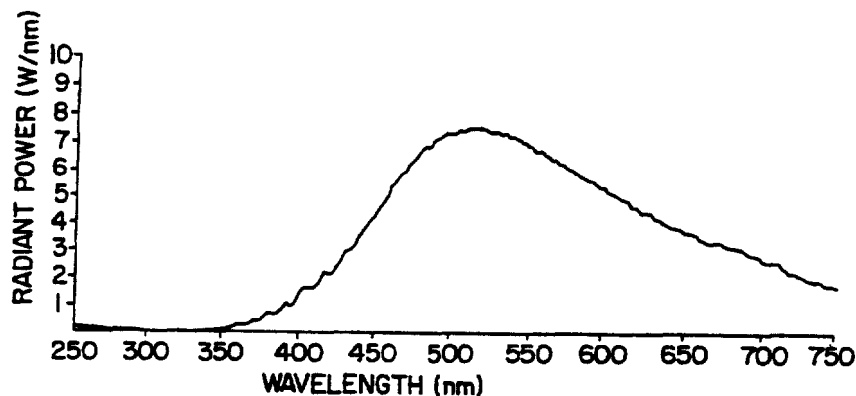
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Primary Examiner—Sandra L. O'Shea*Assistant Examiner*—Mack Haynes*Attorney, Agent, or Firm*—Pollock, Vande Sande & Priddy[57] **ABSTRACT.**

The spectral energy characteristic of a discharge lamp is controlled by changing the density of the fill substance. The spectral characteristic can be shifted while substantially maintaining its shape by changing the density of the fill. A sulfur or selenium containing discharge lamp which is operated at a pressure of at least about 1 atmosphere contains a low ionization potential substance in the fill. Characteristics which are improved are one or more of spatial color uniformity, extinguishing characteristics, and bulb starting reliability. Particular substances which are added to the fill are alkalai metal containing substances, III B metal containing substances, and alkaline earth metal containing substances. When light is reflected back into the bulb, the light which is re-emitted is stronger in the higher wavelengths.

16 Claims, 12 Drawing Sheets

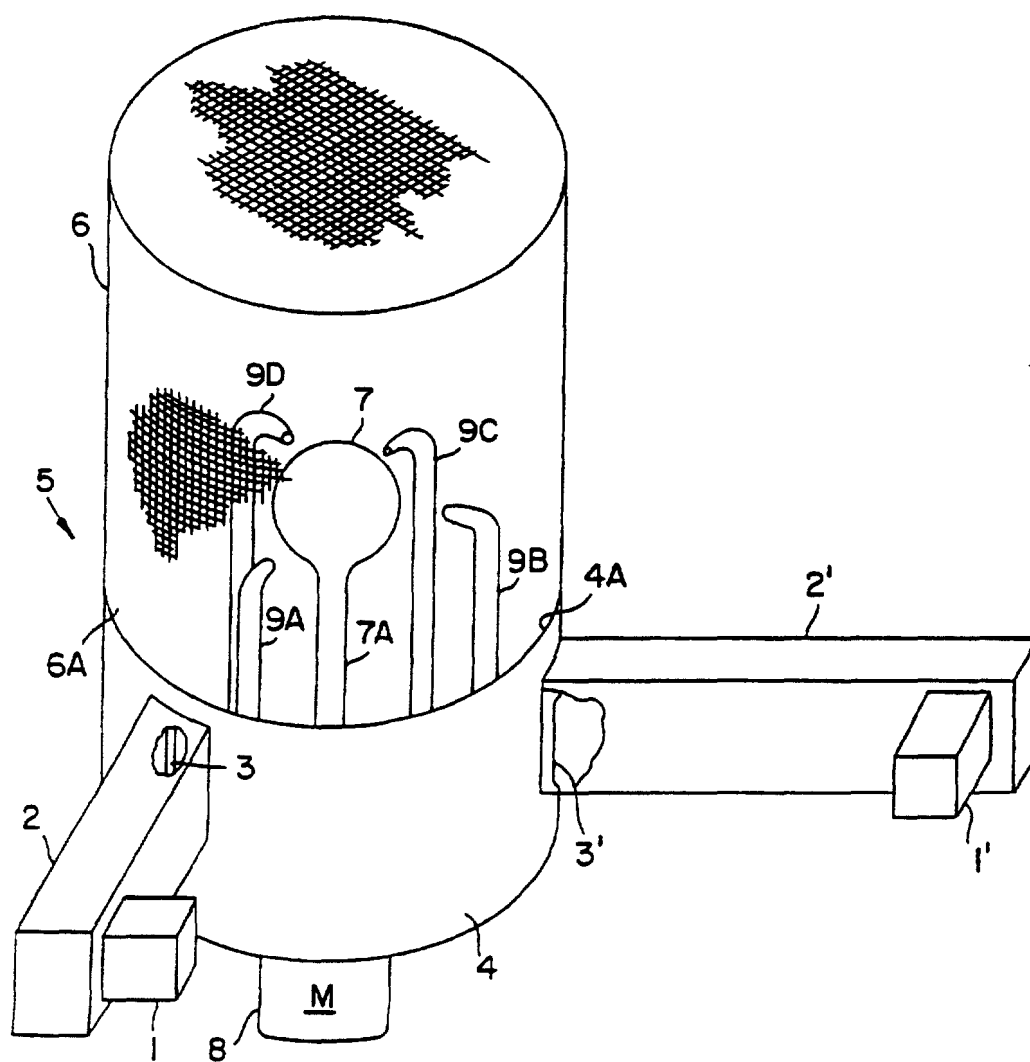


FIG. 2

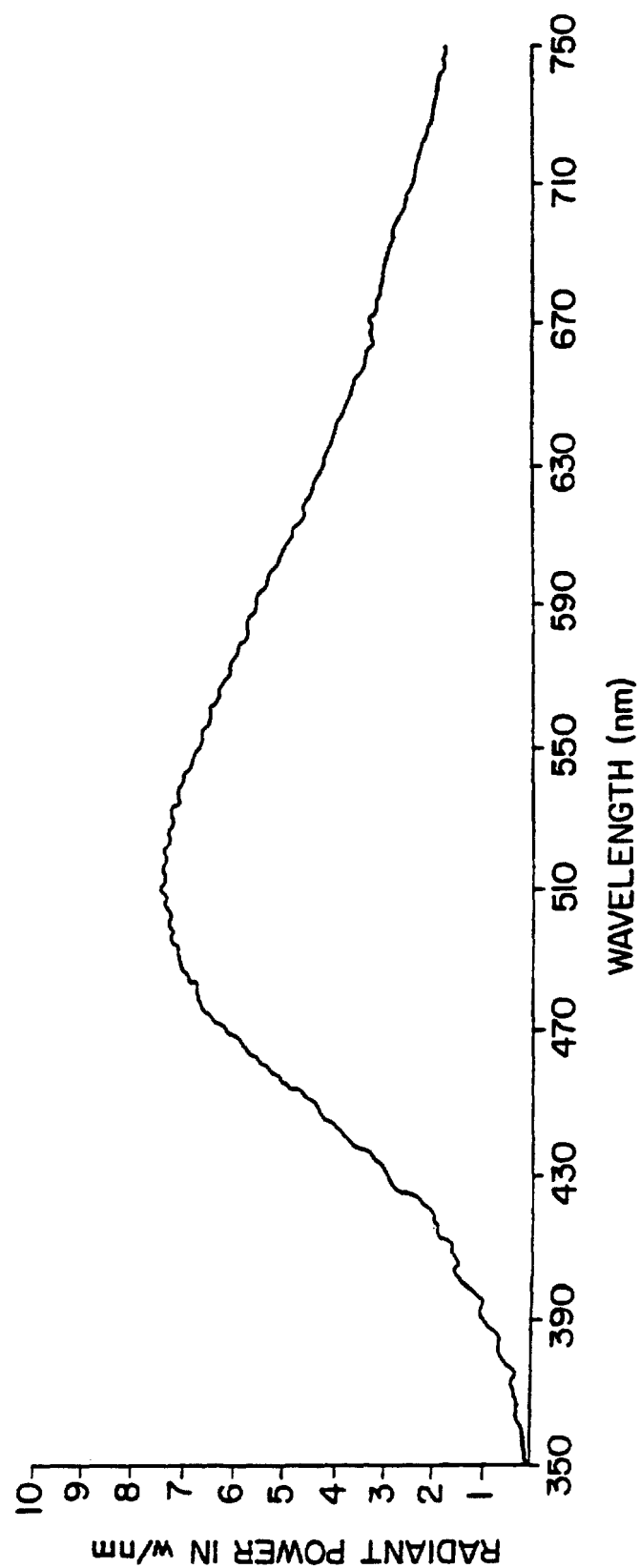
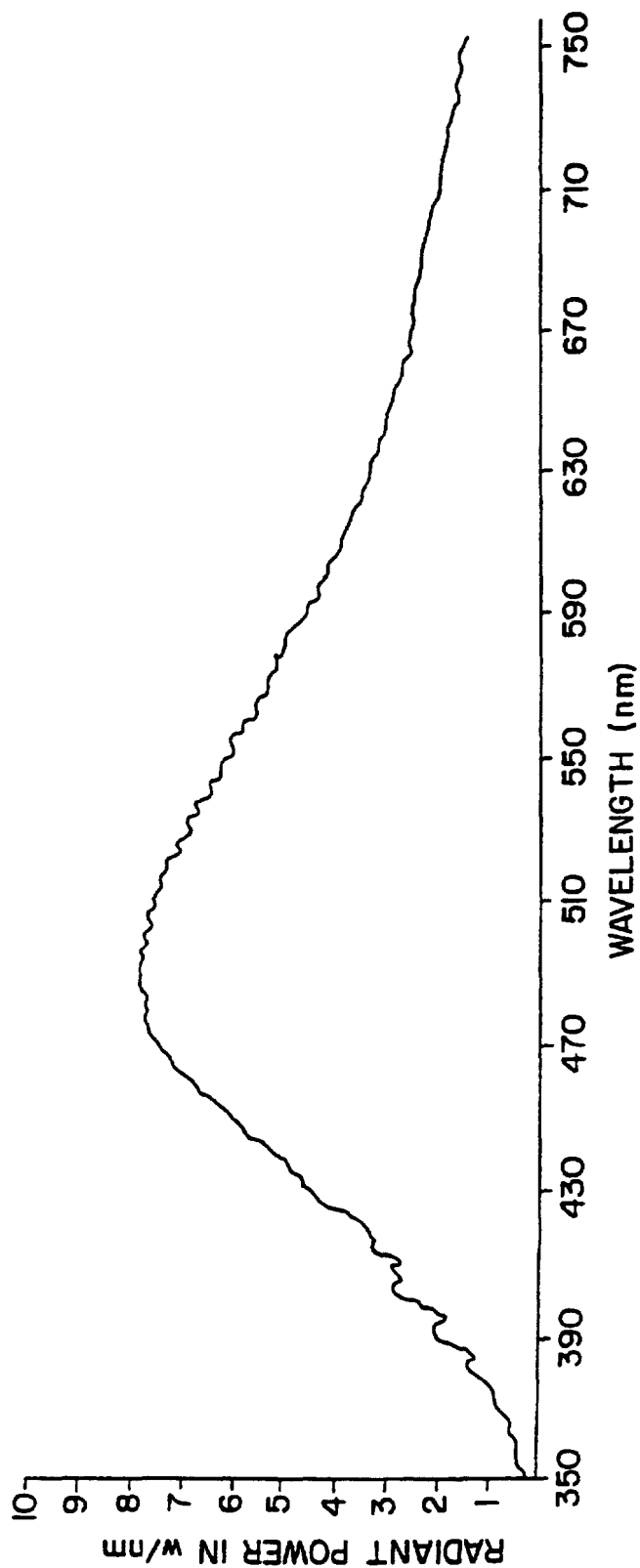


FIG. 3



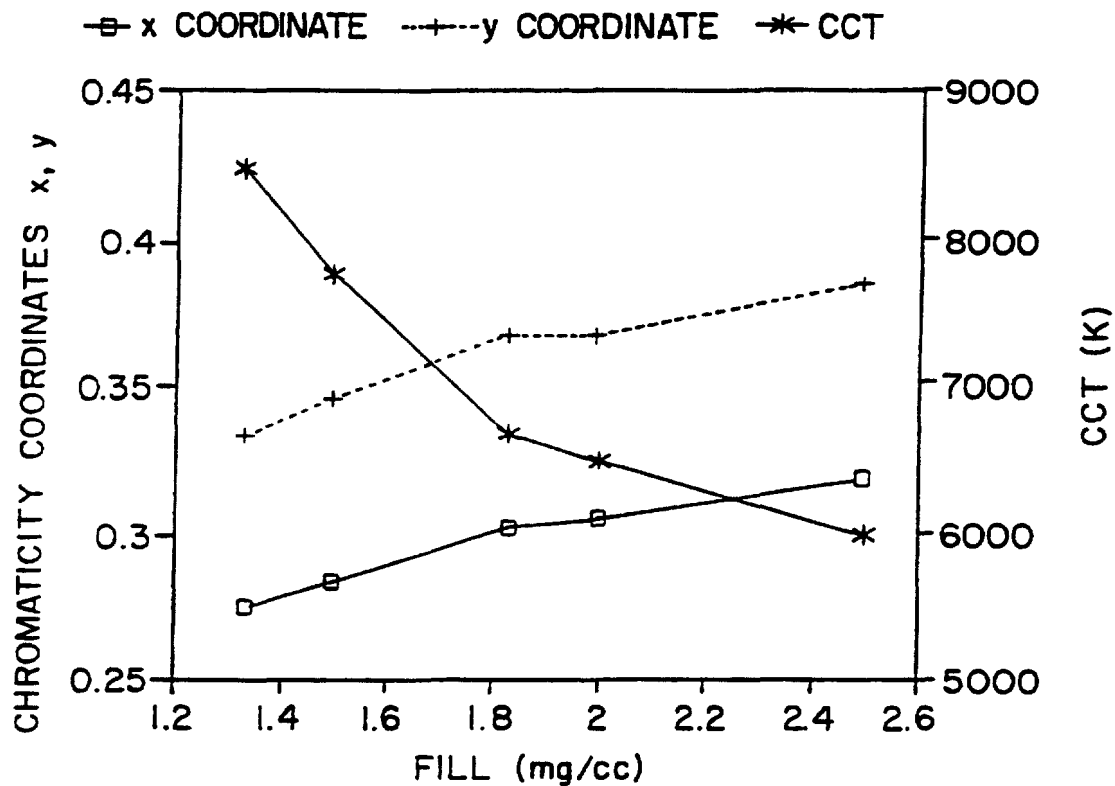


FIG. 4

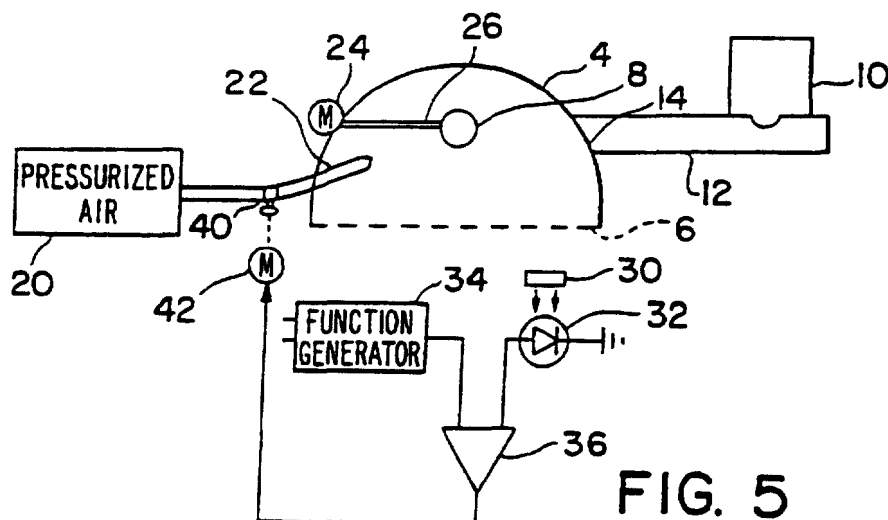


FIG. 5

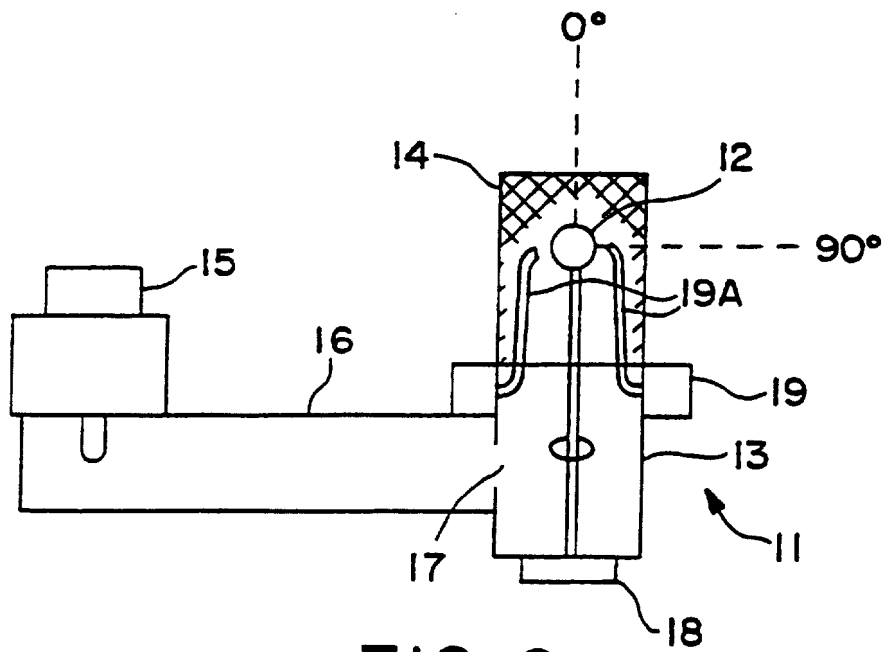


FIG. 6

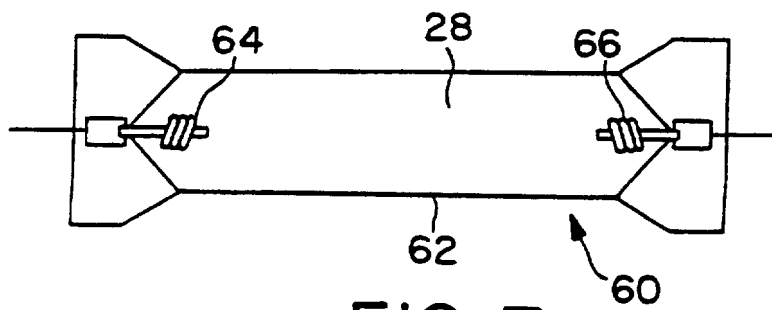


FIG. 7

FIG. 8

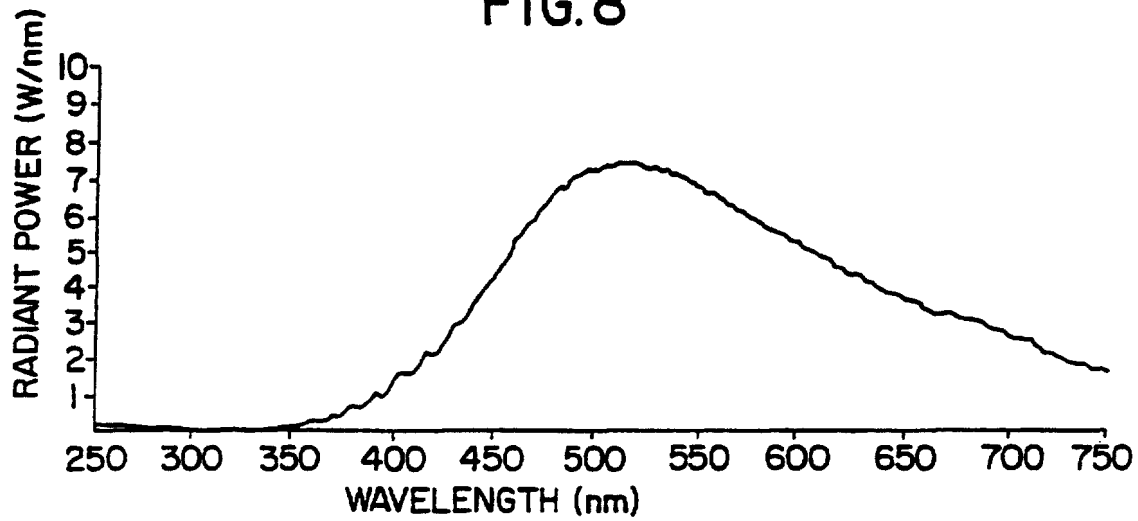


FIG. 9

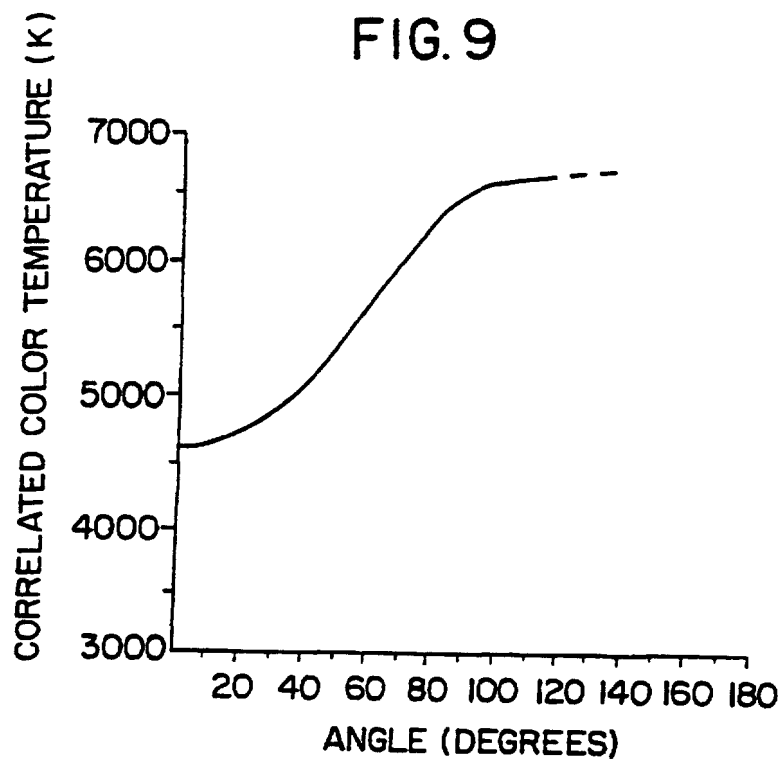


FIG. 10

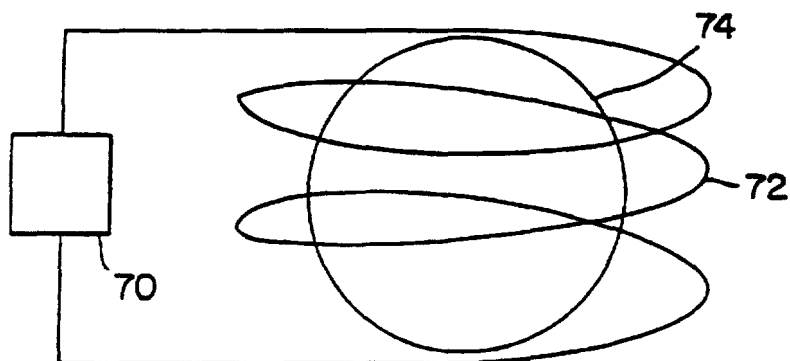
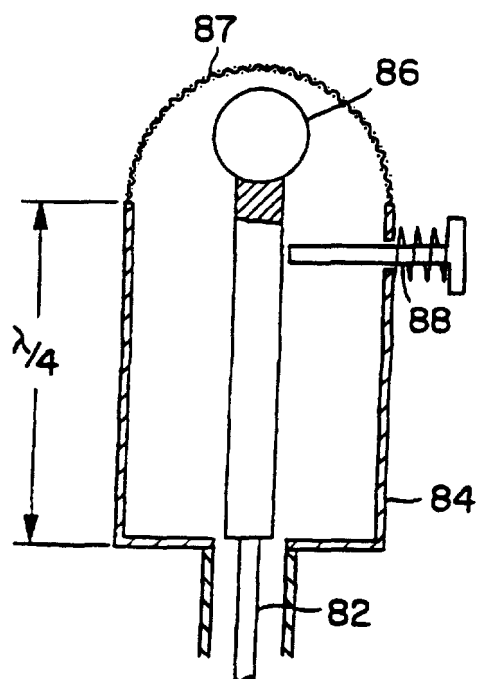


FIG. 11



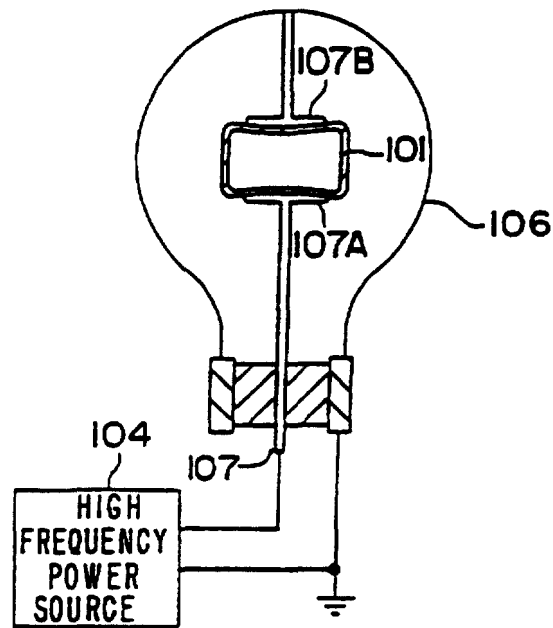


FIG. 12

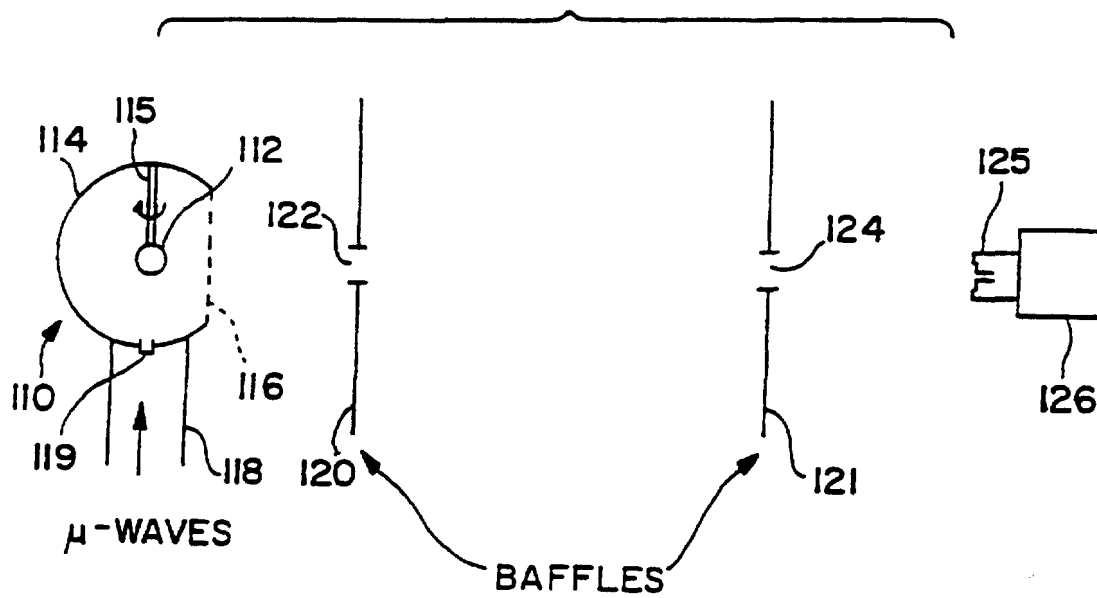


FIG. 13

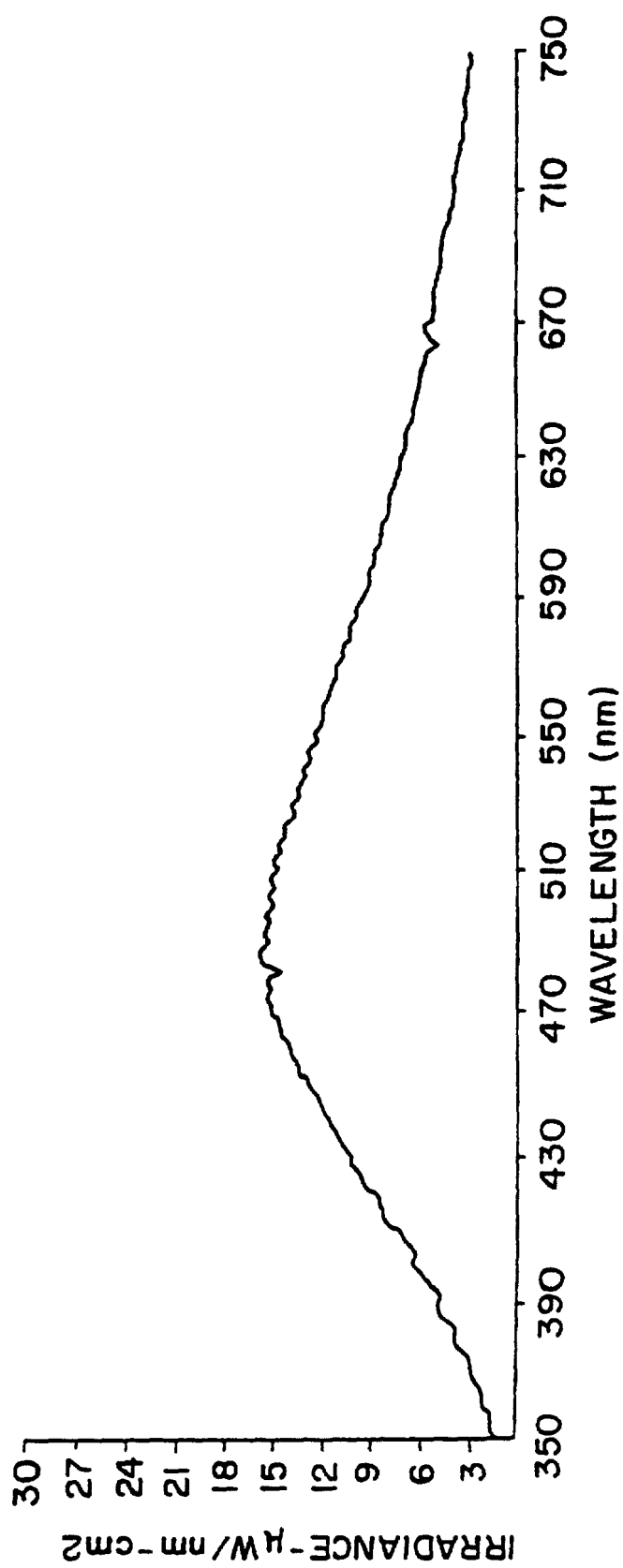


FIG. 14

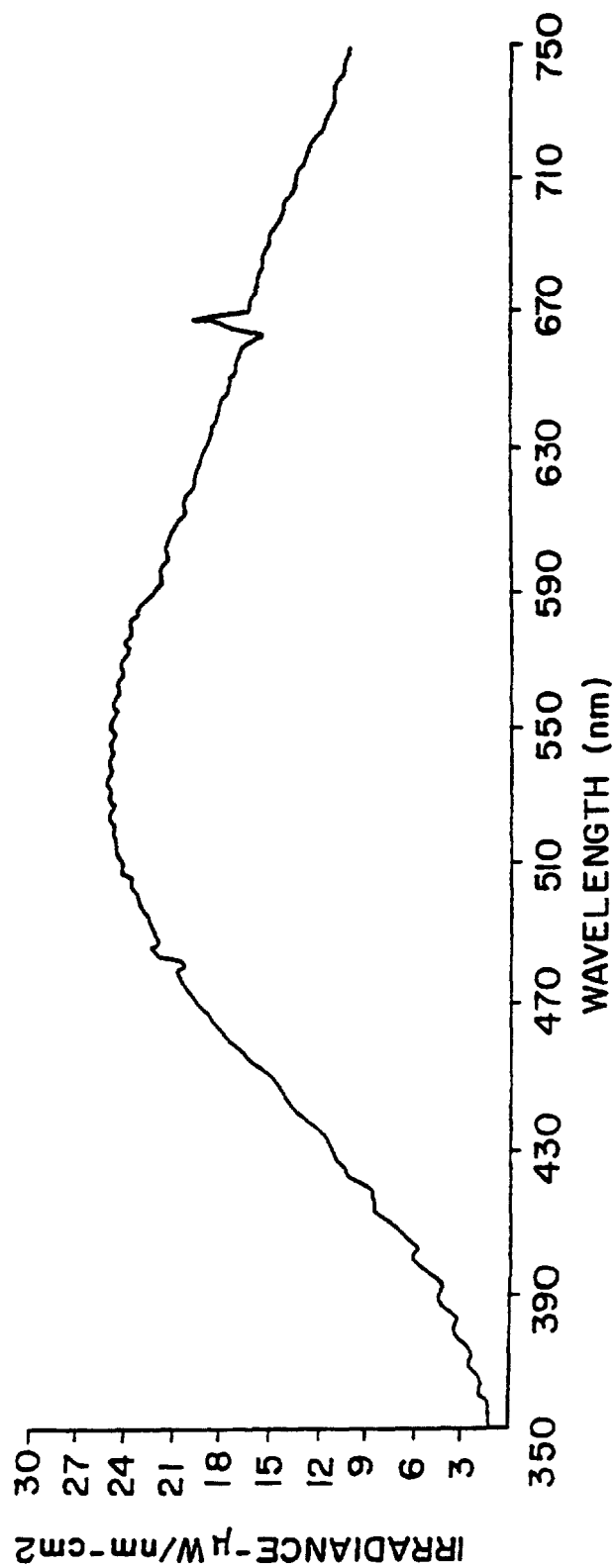
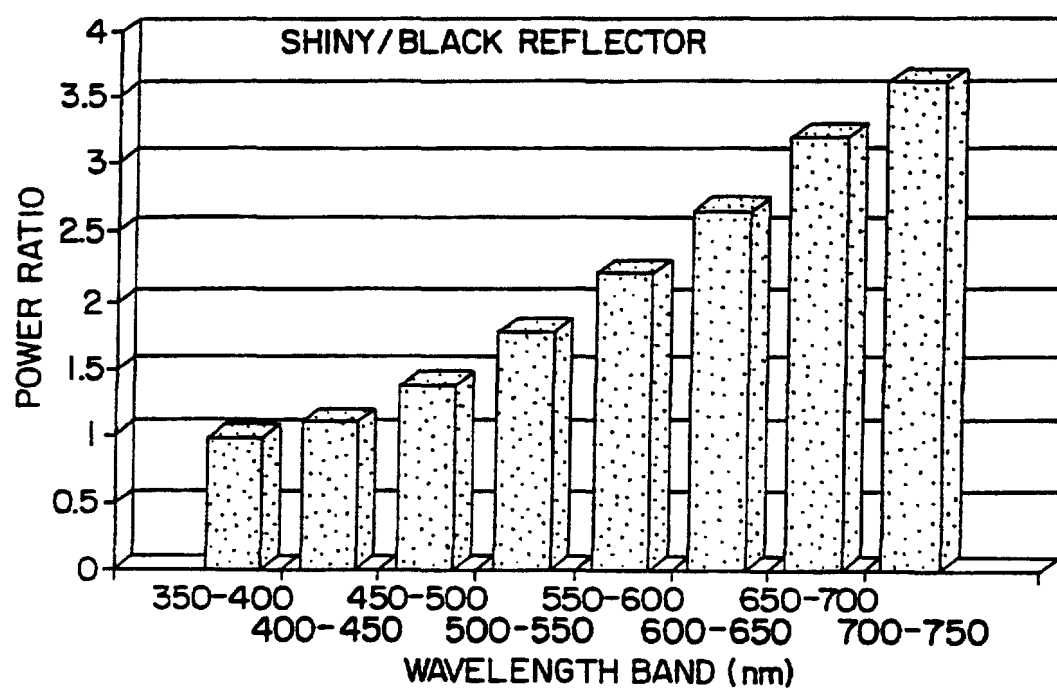


FIG. 15

FIG. 16



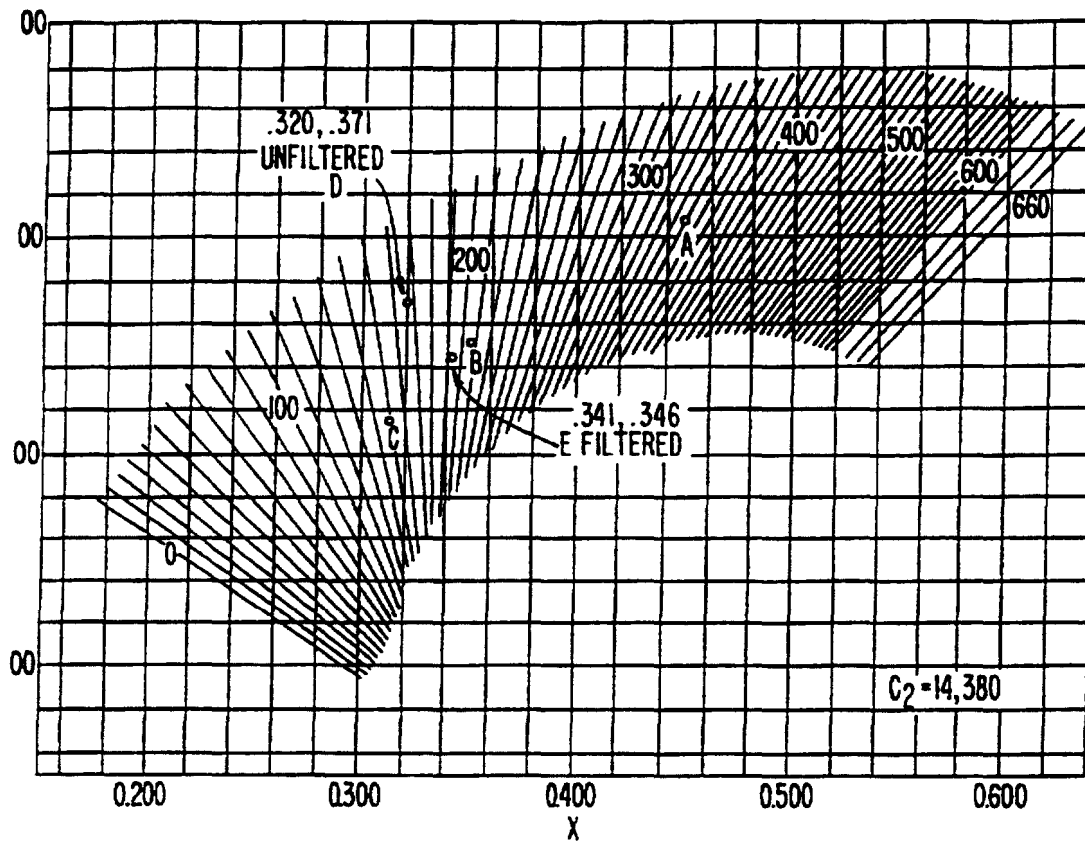


FIG. 17

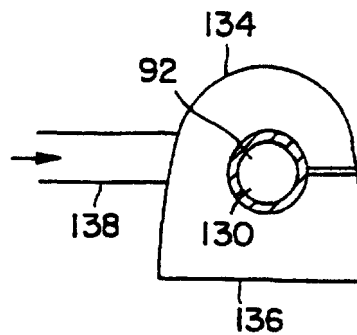


FIG. 18

LAMP WITH LIGHT REFLECTION BACK INTO BULB

CROSS-REFERENCE TO RELATED APPLICATIONS

The present application is a divisional of U.S. application Ser. No. 149,818, filed Nov. 10, 1993, which is a continuation of U.S. application Ser. No. 060,553 filed May 13, 1993, now abandoned, which in turn is a continuation-in-part of U.S. application Ser. No. 867,551, filed Apr. 13, 1992, now abandoned U.S. application Ser. No. 875,769 filed Apr. 29, 1992, now abandoned and U.S. application Ser. No. 882,409, filed May 13, 1992, now abandoned each of which application is a continuation-in-part of U.S. application Ser. No. 07/779,718, filed Oct. 23, 1991, now abandoned which is a continuation-in-part of U.S. application Ser. No. 07/604,487, filed Oct. 25, 1990, now abandoned.

BACKGROUND OF THE INVENTION

One aspect of the present invention relates to an improved visible lamp, and particularly to such a lamp which has a controllable spectral output.

As is well known, the color of the light which is provided by a lamp is determined by the spectral energy distribution of the emitted radiation. In general, visible light sources emit over the spectral range of 350–750 nanometers.

It is desirable to be able to control the "tint" of a lamp which nominally emits over the entire visible spectrum. For example, for certain applications it may be desirable for the light to be tinted red, while for certain other applications, a green tint may be preferred. In addition to being able to provide different lamps having different tints, it is also desirable to be able to vary the tint or spectral emphasis of the light which is emitted by a particular lamp during operation.

In the prior art, discharge lamps are typically provided with different spectral emphases by employing fill additives. For example, a metal halide lamp which is doped with thallium emphasizes the green part of the spectrum, whereas one which is doped with sodium would emphasize the yellow. One disadvantage of such lamps is that a different additive or combination of additives must be used to make each differently tinted lamp, thus introducing manufacturing complexities. Additionally, due to the fact that different fill substances have different aging characteristics, the spectra of lamps using additives are prone to change over time.

Another approach to modifying the color output of a lamp is to use external filters. However, such devices inevitably reduce the efficacy of the overall lamp system. It is also known that incandescent lamps can be made more red by reducing the operating temperature of the filament, but this also has the effect of reducing the lamp efficacy.

Additionally, the above schemes which are known to the prior art change the color emphasis of the light output by changing the shape of the overall spectral distribution, i.e., by emphasizing one portion of the spectrum but not others. However, it has been found that for certain applications, it is advantageous to change the color emphasis while retaining substantially the same shape for the overall spectral distribution. For example, in red/green/blue (RGB) color reproduction systems such as a liquid crystal display (LCD) high definition television, it is desirable to provide a lamp having a spectral energy distribution which can emphasize the blue or red without substantially distorting the shape of the overall distribution.

In U.S. application Ser. No. 779,718, filed Oct. 23, 1991, Ser. No. 604,487, filed Oct. 25, 1990, Ser. No. 882,410, filed May 13, 1992 and Ser. No. 08/071,027, filed Jun. 3, 1993, now U.S. Pat. No. 5,404,076 all of which are incorporated herein by reference, a new type of discharge lamp is disclosed which uses a fill which contains a sulfur or selenium containing substance. The fill is present at a pressure of at least about 1 atmosphere, and is excited at a relatively high power density. The lamp produces a molecular spectrum in the visible part of the spectrum at a relatively high efficacy and has exhibited a long lifetime and a stable color output over time.

While the lamp disclosed in the prior applications has many advantageous properties, when not used in accordance with an aspect of the present invention, the spectral output or color temperature may vary around the periphery of the bulb. It is of course desirable for many applications, for the spectral output to be uniform around the bulb surface, so that all portions of the illuminating energy appear to be the same color.

It has also been found that the above-described spatial "color separation" effect may become more pronounced when the discharge lamp is operated at low power levels. Furthermore, at such power levels the bulb may extinguish or the discharge may retreat from the bulb walls.

SUMMARY OF THE INVENTION

In accordance with a first aspect of the present invention, a discharge lamp is provided which has a fill substance which emits primarily throughout the visible part of the spectrum, and which has the property of having a visible spectral distribution which can be changed by controlling the density of the fill substance.

In accordance with a second aspect of the invention, a discharge lamp is provided which has a fill substance which emits primarily throughout the visible part of the spectrum, and which has the property of having a visible spectral characteristic which can be shifted in wavelength without substantially changing the shape of the characteristic by controlling the density of the fill substance.

In accordance with a third aspect of the present invention, discharge lamps which have a sulfur or selenium based fill are provided with different spectral emphases or tints by controlling the fill density of a sulfur or selenium containing fill substance.

In accordance with a fourth aspect of the invention, discharge lamps having visible spectral characteristics of substantially the same shape, but shifted in wavelength from each other, are provided by controlling the fill density of a sulfur or selenium containing fill substance.

In accordance with a fifth aspect of the invention, the spectral output of a discharge lamp having a sulfur or selenium containing fill is controlled in real time by controlling the fill density during operation. This may be accomplished by controlling the cooling which is applied to the lamp bulb to condense more or less of the fill substance out of the gaseous fill.

Additionally, in accordance with an aspect of the present invention, the bulb fill is constituted so as to obviate the above-described effects of spatially varying spectral output or color temperature. Thus, the lamp may be configured so that it emits with a uniform color temperature around the bulb surface. Additionally, operation at lower power levels without extinguishing may be possible.

In accordance with a sixth aspect of the present invention, a substance is added to the bulb fill which improves the

spatial uniformity of the color temperature of the light which is emitted by the bulb.

In accordance with a seventh aspect of the invention, a substance is added to the fill which improves the starting of the lamp.

In accordance with a eighth aspect of the invention, a substance is added to the fill which allows the lamp to be effectively operated at lower power levels.

In accordance with a ninth aspect of the invention, a substance is added to the fill which has a low ionization potential.

In accordance with a tenth aspect of the invention, a substance is added to the fill which is an alkalai metal containing substance.

In accordance with a eleventh aspect on the invention, a substance is added to the fill which is a III B metal containing substance.

In accordance with a twelfth aspect of the invention, a substance is added to the fill which is an alkaline earth metal or a rare earth element containing substance.

In accordance with a thirteenth aspect of the invention, mercury is added to the fill.

In accordance with a fourteenth aspect of the invention, an improved bulb is provided, which may be used in a discharge lamp.

It is known in the prior art to add the substance sodium, which is an alkalai metal, to discharge lamps to provide spectral emphasis, and to arc lamps in particular to rectify a problem known as "arc constriction" wherein the discharge between the electrodes becomes undesirably constricted in certain regions.

It has been discovered in accordance with the present invention that when a low ionization potential material is added to the fill of a high pressure lamp containing sulfur or selenium, the spatial uniformity of the color temperature of the light emitted by the bulb and/or the starting characteristics of the lamp are improved.

It has further been discovered that when an alkalai metal containing substance is added to the fill of a high pressure lamp wherein the primary light emitting fill component is a sulfur or selenium containing substance, the following advantages are provided:

- a) the color temperature of the emitted light around the surface of the bulb becomes spatially more uniform, and this is in general true even at lower power densities;
- b) the lamp starts more reliably; and
- c) the lamp may be operated at lower power levels without extinguishing.

Additionally, it has been discovered that when a III B metal containing substance is added to the lamp fill of a high pressure sulfur or selenium containing lamp, the spatial uniformity of the color temperature of the emitted light around the bulb is improved.

In accordance with a still further aspect of the present invention, it has been found that when the light which is emitted by a sulfur or selenium based discharge lamp is reflected back into the bulb, the resultant light which is re-emitted is stronger in the higher wavelengths, i.e., the red portion of the spectrum. Therefore, by using a reflector which is approximately spherical in shape, a lamp which is richer in red wavelengths may be provided. Additionally, by using a wavelength selective reflector, such as a dichroic reflector, a lamp having a spectral output which is more nearly equivalent to that of a black body may be provided. Also, by the use of such wavelength selective reflectors, lamps which are well suited to particular applications may be provided.

The invention will be better understood by referring to the accompanying drawings wherein:

BRIEF DESCRIPTION OF THE FIGURES

FIG. 1 shows a microwave powered electrodeless lamp.

FIG. 2 shows a spectral energy distribution with a peak at 515 nanometers.

FIG. 3 shows a spectral energy distribution with a peak at 490 nanometers.

FIG. 4 shows a graph of wavelength peak vs. fill density.

FIG. 5 shows a system wherein the fill density is controlled by varying the cooling of the lamp.

FIG. 6 shows a further embodiment of a high pressure sulfur or selenium containing lamp.

FIG. 7 shows a further embodiment of a sulfur or selenium containing lamp.

FIG. 8 shows a exemplary spectrum emitted by the lamp of FIG. 6.

FIG. 9 is a graph of correlated color temperature vs. angular position for a lamp such as is shown in FIG. 6.

FIG. 10 shows a further embodiment of a lamp which may incorporate the invention.

FIG. 11 and 12 show further embodiments of sulfur or selenium based discharge lamps.

FIG. 13 shows a lamp with a spherical reflector in a spectrum measuring setup.

FIG. 14 shows the spectrum obtained with the arrangement of FIG. 13 when the reflector is blackened.

FIG. 15 shows the spectrum obtained with the arrangement of FIG. 13 when the reflector is shiny.

FIG. 16 is a graph depicting the power ratios of shiny/black reflectors by wavelength range.

FIG. 17 is a 1931 chromaticity diagram depicting coordinates of an uncorrected and corrected lamps respectively.

FIG. 18 shows a further embodiment of the invention.

DETAILED DESCRIPTION OF THE INVENTION

FIG. 1 shows a microwave powered electrodeless lamp into which the present invention may be incorporated. Referring to the figure, a pair of magnetrons 1, 1' generate microwave energy which propagates along waveguides 2, 2'. The waveguides lead to microwave cavity 5 which is comprised of solid conductive wall, cup-shaped part 4, and metal mesh cupshaped part 6, which are joined at their respective ends 4A, 6A. Within the end of the waveguides 2, 2', on the solid wall are located antenna slots 3, 3' which serve to couple microwave energy from the waveguide into the cavity where it causes an oscillating field to occur.

A discharge bulb 7 including a supporting stem 7A is located within cavity 5. The supporting stem is connected through a hole (not shown) in solid cup shaped part 4, to the shaft of a motor 8. The motor rotates the bulb 7 to improve the cooling of the bulb.

As mentioned above, the fill in bulb includes a sulfur or selenium containing substance. It is further desirable to use an inert gas, such as argon or xenon, which aids in starting the discharge. The lamp of FIG. 1 may be characterized as a high pressure lamp. Thus, the fill in bulb 7 is present in amounts such that the fill pressure is at least 1 atmosphere or above when excited to operating temperature, and is preferably 2 to 20 atmospheres. Furthermore, the fill pressure is mainly controlled by the primary radiating

component, which typically has a substantially higher partial pressure than that of other constituents when the lamp is operational. The illumination provided by the lamp may be augmented in various regions of the spectrum by including certain additives in the fill.

As noted above, in addition to using sulfur and selenium in elemental form, compounds of these elements may be used. For example, InS , As_2S_3 , CS_2 , SeO_2 , SeCl_4 , and HgSe , as well as other compounds of sulfur and selenium, may be used. The compounds which are used have a low vapor pressure at room temperature, i.e., they are in a solid or liquid state, and a high vapor pressure at operating temperature.

The term "a sulfur containing substance" as used herein, includes both elemental sulfur and sulfur compounds, while the same is true for the corresponding terms as applied to selenium. It should be appreciated that the primary radiating component of the fill may be comprised of a combination of a sulfur containing substance and a selenium containing substance, rather than only one of these substances. Additionally, the primary radiating component may be comprised of a mixture of the elemental form and a compound(s) of a particular substance or substances.

The fill is excited at power densities in excess of 50 watts/cc and preferably in excess of 100 watts/cc. As stated in application Ser. Nos. 779,718 and 882,410 in the computation of power density, the volume, refers to the volume of the light emitting gas rather than to the volume of the bulb.

Referring to FIG. 2, the spectral energy distribution of a lamp as shown in FIG. 1 is shown. The spectral energy distribution covers the range from 350 to 750 nanometers, which is generally the visible range. The spectrum has its peak at about 515 nanometers, and the output appears to be white with a green tint. As is seen, the spectrum is continuous throughout the visible range. Analyses of the spectral energy distribution according to the 1931 CIE (Commission International de l'Eclairage) determines a correlated color temperature of 6000 degrees kelvin and x and y coordinates of 0.320 and 0.386 respectively on the chromaticity diagram. The bulb which provided the spectrum which is shown in FIG. 2 was provided with a discharge fill consisting of 2.5 milligrams per cubic centimeter of sulfur, and 60 torr of argon.

Referring to FIG. 3, the spectral energy distribution of a second lamp made and operated according to the invention is shown. This lamp was operated under the same conditions as the lamp represented in FIG. 2, but the lamp represented in FIG. 3 was provided with sulfur of somewhat lesser density than the lamp represented in FIG. 2, that is 1.3 milligrams per cubic centimeter. This bulb also had 60 torr of argon. The output appears white but in this case with a blue tint, and the peak of the spectral energy distribution occurs at about 490 nanometers. The correlated color temperature is 8500 degrees kelvin, while the x and y coordinates on the chromaticity diagram are 0.275 and 0.334 respectively.

It should be noted that both of the spectra shown in FIGS. 2 and 3 ascend from near zero smoothly from the 350 nanometer mark to their respective peaks, and descend more gradually to a low level at the 750 nanometer mark. Aside from the slight jitter, the curves are smooth. This is in contrast to the ubiquitous variants of metal halide lamps which exhibit strong line spectra. Additionally, it is significant to note that the shape of the spectrum is substantially preserved between the first and the second spectra. However,

due to the spectral shift, it will be seen that the amplitude of the spectrum shown in FIG. 2, which peaks at 490 nanometers is higher at the lower wavelengths and lower at the higher wavelengths than that shown in FIG. 3, which peaks at 515 nanometers.

Although the spectral energy distributions which are shown in FIGS. 2 and 3 are significantly shifted from each other, they by no means represent the extremes in what is available in the practice of the invention. That is, lesser or greater amounts of fill can be used to achieve shifts in the spectrum toward shorter or longer wavelengths respectively. This is illustrated in FIG. 4, which is a graph of peak wavelength vs. sulfur density for the lamp which is shown in FIG. 1.

With regard to the choice between a sulfur containing substance, a selenium containing substance or combinations thereof, the following is to be noted. For a given fill density sulfur will provide a higher color temperature and selenium a lower color temperature. Furthermore, a fill in which a combination of sulfur and selenium is used has the advantage that higher total vapor pressures can be obtained from the two somewhat independent partial pressures, and a further shift to the red can be obtained. Additionally, it has been determined that a fill comprising a mixture of sulfur and selenium provides a spectrum having a shape as shown in FIGS. 2 or 3. It is contemplated that the relative shift of the spectrum attained with a bulb using both materials in the fill can be controlled between the extremes of fills containing the only one of the materials by selecting the ratio of sulfur and selenium in the fill. Increasing the sulfur density and decreasing the selenium density will raise the color temperature, and vice versa.

As mentioned above, such lamps may have particular applicability to a red/green/blue (RGB) color display system. The region of the chromaticity diagram extending from about 0.200 to about 0.490 on the x axis, and about 0.200 to about 0.450 on the y axis is white light, while various subregions will have a discernable tint. A source which falls within the white region is suitable for use in an RGB color system in which the light from the source is separated into the three primary color beams which are modulated image-wise and recombined to form a color image. It is however, desirable to be able to shift the spectrum while preserving its shape in order to provide an optimum spectrum for a particular RGB system.

The lamp of the present invention has particular utility as a projection source, for example, for use in high definition television.

According to another embodiment of the invention, the spectral energy distribution of a particular lamp can be controlled during lamp operation. In this embodiment the effective fill density is changed by increasing the cooling of the bulb, such as by increasing the pressure of the cooling air which is delivered to cooling jets 9A, 9B, 9C, 9D in FIG. 1 to the point that some of the fill in the bulb condenses on the inside of the envelope and ceases to participate in the discharge. A bulb may be modified to provide a special area or a side pipe may be provided in which the fill material will be selectively caused to condense. In this way the condensed fill will not interfere with the light emission from the bulb. The special area may simply be a certain area of an unmodified standard shaped bulb which is provided with augmented cooling. For example in the lamp shown in figure one the cooling jet 9A which cools the lowest part of the bulb, whereat the stem is connected, may be operated at higher air pressure. In this way, fill condensation will occur at that area

of the bulb which is out of the way of the emission directed at towards the lamps optics. Although not shown the optics may comprise a reflector with its optical axis coincident with the cylindrical axis of the cavity.

A system for controlling bulb temperature is shown in FIG. 5, which appears in U.S. Pat. No. 4,978,891, which is incorporated herein by reference.

Referring to FIG. 5, filter 30 is provided and is located so as to receive light from the lamp. Filter 30, for example, may be a band pass filter which transmits light only in the blue region of the spectrum, and is followed by photodetector 32 which generates a comparison signal.

Function generator 34 is also provided, which is capable of generating a preselected function signal of desired, arbitrary shape. The outputs of photodetector 32 and function generator 34 are fed to comparator 36, which generates a difference signal. This difference signal is fed back to the cooling fluid supply system to control the amount of cooling fluid impinging on the bulb.

For example, in FIG. 5, an exemplary control for the cooling fluid supply is a needle valve 40, the position of which is controlled by stepping motor 42. Alternatively, the input to pressurized air supply 20 could be throttled or the supply could be vented, to control cooling.

Thus in accordance with this embodiment, whenever the output in the blue region is different than that which has been programmed by function generator 34, a difference signal results, which causes the cooling of the lamp bulb 8 to vary, until the difference signal is at or approaches zero.

Another method of changing the shifting spectrum would be to vary the power while maintaining constant cooling. This would result in partial condensation of the fill and would change the effective fill density in the bulb resulting in a shift of the spectral energy distribution.

A combination of sulfur and selenium containing fill substances can be advantageously used in the embodiments in which the spectrum is shifted during operation (see FIGS. 2, 3). Sulfur has a higher vapor pressure as well as a somewhat higher color temperature. As a discharge bulb containing both sulfur and selenium is cooled to the point that a portion of the fill condenses on the bulb 7 wall, the overall operational fill density will be lowered leading to a higher color shift (i.e. by way of a shift of the spectrum to the blue). A second compounding effect is that the selenium will condense out faster leaving an effective operating fill which has more sulfur, which by its nature gives a higher color temperature.

It should be noted that as used herein, the term "primary radiating component" means that fill component which provides a radiation output which is at least as great as any other fill component.

It should be understood that the above embodiments have been illustrated in connection with specific lamps, but that other specific lamp structures may be used as well. For example, the shape of the microwave cavity as well as the microwave coupling schemes may be varied, and the invention is also applicable lamps which are powered with radio frequency (r.f.) energy, as well as to arc lamps.

While one advantage of the invention is that it provides a lamp which is capable of operating without using mercury, the addition of a small amount of mercury may help lamp starting. Additionally, for those applications where the presence of mercury is not considered to be a problem, it has been found that the addition of more substantial amounts of mercury increases efficiency significantly.

For example, in a bulb of 5 mm ID (6 mm OD), having a volume of 6.5×10^{-2} cc, a mercury dose of about 5 mg was added to a sulfur dose of about 0.33 mg, and 150 torr of argon. The pressure of the mercury vapor at operating temperature was about 90 atmospheres.

At 570 watts microwave input power input, the addition of the mercury resulted in an 11% improvement in efficacy, and had a significantly lower cooling requirement, which allows a less noisy pressurized cooling air source to be used. Such a lamp would be suitable for uses as a projection lamp.

In accordance with a further embodiment, xenon is used as the inert gas, and is present at partial pressure during operation which is less than but comparable to the sulfur partial pressure within an order of magnitude, or a partial pressure which is greater than the sulfur partial pressure. This arrangement results in increased efficacy.

For example, a bulb of 28 mm ID was filled with 24 mg of sulfur and 400 torr of xenon at room temperature. An increase in efficacy of 6% was realized over the case where 60 torr of argon was used as the inert gas.

Referring to FIG. 6, a lamp embodiment which is used to illustrate a further aspect of the present invention is depicted. Lamp 11 is an electrodeless lamp which is powered by microwave energy. Bulb 12, which contains a high pressure fill, and is made of quartz or other suitable material, is supported in a microwave cavity, which is comprised of conductive housing 13 and mesh 14. Magnetron 15 generates microwave energy, which is fed by waveguide 16, to coupling slot 17 of the microwave cavity.

This excites the bulb fill to a plasma state, whereupon light is emitted by the fill, which is transmitted out of the cavity through mesh 14. The mesh is metallic, and is constructed so that it is substantially opaque to microwave energy, while being substantially transparent to the light which is emitted by bulb 12. The bulb is rotated by rotator 18, and the bulb envelope is cooled by gas which is fed in to plenum 19 and out through nozzles 19A.

A further embodiment of a lamp is shown in FIG. 7. This is an arc lamp 60 which is comprised of quartz envelope 62 having electrodes 64 and 66, and containing fill 28. To excite the fill, an A.C. voltage is impressed across the electrodes, whereupon an arc discharge occurs therebetween.

As in the case of the electrodeless lamp, the fill contains a sulfur or selenium containing substance which is present at a high pressure of at least about 1 atmosphere and preferably in the range of about 2-20 atmospheres. An electrical voltage is applied across the electrodes such that a suitably high power density exists. Additionally, the electrodes 64 and 66 are made of or plated with a special material, to prevent chemical reactions with the fill gas which may lead to electrode deterioration.

The sulfur and selenium containing lamps described herein radiate a molecular spectrum in the visible region. A representative spectrum is depicted in FIG. 8 and is seen to be smooth, with the sharp peaks which are characteristic of atomic spectra being notably absent. The spectrum shown in FIG. 8 resulted when an electrodeless lamp such as is shown in FIG. 6 having a bulb of spherical shape of internal diameter 2.84 cm was filled with 0.062 mg-moles/cc of sulfur and 60 torr of argon, and was excited with microwave energy at a power density of about 280 watts/cc.

It has been observed that while light having the spectrum which is shown in FIG. 8 would be emitted from somewhere on the surface of the bulb, light having the identical spectrum would not in general be emitted from every point on the surface of the bulb. An accepted way of expressing spectral

output is in terms of "color temperature" or "correlated color temperature", and thus stated differently, it was found that the color temperature or correlated temperature of the light varied as a function of the angle from which the bulb is observed. This is depicted in FIG. 9, which is a graph of correlated color temperature vs. observation angle. It is seen that as one progresses from the 0° line shown in FIG. 6, through the 900 line, and then on to a displacement of 180°, the color of the emitted light changes. As mentioned above, for many applications, a bulb with a spatially uniform color temperature would provide a better result. Additionally, the phenomenon of spatial "color separation" becomes more pronounced as the power level of the excitation energy decreases, either by virtue of dimming the lamp, or operating it at a lower power. It was also found that it may not be possible to dim the lamp as much as is desired, since the lamp may extinguish when a low power threshold is crossed.

It was further found that the above-described sulfur and/or selenium containing lamps do not always start in a fast and reliable fashion. In the case of the lamp shown in FIG. 6, it is standard to use a supplemental light source to provide additional energy to initiate starting. However, even with the use of such supplemental light source, starting may not always be reliable.

In accordance with an aspect of the present invention, a substance is added to the bulb fill which has a low ionization potential. Such a substance has electrons which are loosely bound, thereby making them easy to dislodge. It has been found that when such a substance is added to the bulb fill, one or more of the uniformity of the color temperature, bulb extinguishing characteristics, and bulb starting characteristics, are improved.

One class of low ionization potential materials are the alkali metals, and it has been found that when an alkali metal containing substance is added to the fill, the following advantages result:

- a) the color temperature of the emitted light around the surface of the bulb becomes spatially more uniform, and this is in general true even at lower power densities;
- b) the lamp starts more reliably; and
- c) the lamp may be operated at lower power levels without extinguishing.

The alkali metals may be used in either elemental or compound form, and one such substance which may be used is sodium. Other alkali metals are lithium, potassium, rubidium, and cesium. By way of non-limitative examples, compounds in the form of halides or sulfides may be used, for example NaI, Na₂S or LiI. Adding a sodium containing substance to the bulb fill may also have the effect of providing spectral emphasis in the red part of the spectrum.

Another class of low ionization potential materials are the III B metals. It was found that when a III B metal containing substance was added to the fill, the color temperature of the emitted light become more uniform, and this is in general true even at lower power densities. Furthermore, it is possible to operate the lamp at lower power levels without extinguishing. The III B metals include indium, thallium, gallium, aluminum, and may be used in elemental or compound form, for example combined as halides such as InI, TlI, TlBr, or combined as sulfides such as InS, Tl₂Se, or Tl₂S.

A further grouping of low ionization materials are the alkaline earth or rare earth elements. Such substances cause the lamp to start more reliably. The alkaline earth metals are barium, beryllium, magnesium, calcium, strontium, and radium, and they may be used in elemental or compound

forms, for example combined as halides such as CaBr₂, BaI₂, SrI₂ and sulfides, such as CaS, BaS, BaSe. The rare earth elements are yttrium, scandium, and lanthanum through lutetium. The improved starting is due to the low work functions of the alkaline earth and rare earth elements.

It was further found that the addition of mercury to the bulb improved starting reliability.

The amount of the above-mentioned additives to be used to produce optimum results for different applications may vary. For example, for the lamp desired above which produced the spectrum of FIG. 8, Na may be added in an amount of at least 0.001 mg/cc, In may be added in an amount of at least 0.01 mg/cc, and Ba may be added in an amount of at least 0.005 mg/cc. Additives may produce spectral emphasis, so that the resultant spectrum may not be identical to that shown in FIG. 8. In the case of mercury, at least 0.1 mg/cc should be used. It may also be possible to use a combination of the additives disclosed herein together in the lamp fill. It is further noted that since some of the above-mentioned additives improve lamp starting, it may be possible, in certain implementations, to eliminate the inert gas constituent of the fill.

The following Examples are illustrative:

EXAMPLE I

In a lamp as shown in FIG. 6, a bulb which is 2.84 cm in interior diameter was filled with 24 mg of S (2 mg/cc) and 60 torr of Ar., and operated at a suitably high power density. A figure of merit identified as "uniformity", is defined as the ratio of the minimum to maximum intensity of the light outputted by the bulb considering all angular positions except where the bulb is obstructed, e.g., by a narrow screen ring. The reason that the "uniformity" is a figure of merit representative of the color separation effect is that for lamps of this type, regions of lower color temperature also have lower output. The uniformity for the lamp was found to be 0.81.

EXAMPLE II

A lamp as described and operated in connection with Example I was filled with 24 mg of S (2 mg/cc), 60 torr of Ar., and 0.2 mg of NaI (0.017 mg/cc) which contained 0.031 mg (0.0026 mg/cc) of Na. The "uniformity" was 0.97, and a uniform color temperature around the angular extent of the bulb could be visually observed.

EXAMPLE III

A lamp as described and operated in connection with Example I was filled with 24 mg of S (2 mg/cc), 60 torr of Ar., and 0.3 mg of InI (0.025 mg/cc) containing 0.143 mg (0.012 mg/cc) of In. The "uniformity" was 0.91.

EXAMPLE IV

A lamp as described and operated in connection with Example I was filled with 24 mg of S (2 mg/cc), 60 torr of argon, and 1 mg (0.083 mg/cc) of BaS containing 0.81 mg (0.068 mg/cc) of Ba or instead of the BaS, 7 mg of Hg. An improvement in the starting reliability of the lamp was observed.

It should be noted that in term "power density", the volume (cc) refers to the volume of the light emitting gas rather than to the volume of the bulb. Further, it should be noted that the term "operating temperature" as used herein is the temperature which is attained by the bulb during operation.

It is significant that when fill additives as discussed herein are used it may be possible to operate the lamp at significantly lower power densities than indicated above without causing objectionable color separation or bulb extinguishment.

A further embodiment of the invention is shown in FIG. 10, which is an illustrative example of a lamp which is excited with electromagnetic energy in the radio frequency range. In this regard, the term "electromagnetic energy" as used herein refers to both microwave and r.f. modes.

Referring to FIG. 10, r.f. source 70 generates r.f. power which is fed to induction coil 72. Bulb 74, which houses a sulfur or selenium containing fill as described above also includes additives which may include an alkali halide containing substance or a III B metal containing substance as discussed above. In the operation of the lamp, r.f. energy from the induction coil 72 is coupled to the bulb fill, thereby exciting it to produce a spectrum in the visible range as previously described. The additives mentioned above permit operation at lower power densities, which in general is a significant advantage, and may be a particular advantage in the use of r.f. lamps. The invention may be applied to the different types of r.f. lamps, which include by way of non-limitative example, inductively and capacitively coupled lamps.

As is well known to those skilled in the art, the particular form of the electrodeless lamp heretofore described is exemplary only, and other specific shapes and types of cavities, for example, substantially all mesh type, as well as different types of coupling modes using one or more power sources, and one or more waveguides or other coupling modes may be used.

For example, FIG. 11 illustrates a lamp wherein coupling is effected in a coaxial mode. Microwave power is provided to inner and outer conductors 82 and 84 for coupling to bulb 86. A conductive mesh 87 is connected to the outer conductor. A tuning element 88 may be provided to help in starting the lamp.

FIG. 12 depicts a further embodiment which is powered by r.f. or microwave power. Power from high frequency power source 104 is coupled to inner conductor 107 and outer conductor 106, which is a conductive mesh, the bulb 101 is supported between inner conductive member 107A and inner conductive member 107B. The embodiment shown in FIG. 12 may be considered to be a form of capacitive coupling.

As discussed above, the sulfur and selenium containing lamps described herein radiate a molecular spectrum in the visible region. A representative spectrum is smooth, with the sharp peaks which are characteristic of atomic spectra being notably absent.

FIG. 13 depicts an embodiment of the invention wherein electrodeless lamp 110 is shown which has a fill wherein a sulfur containing substance or a selenium containing substance is the primary radiating component, as described above. Bulb 112 is secured in approximately spherical reflector 114 by bulb stem 115. The bulb stem may be arranged for rotation while streams of cooling fluid are directed at the bulb, to effect cooling (not shown). A mesh 116 contains microwave energy while allowing the emitted light to escape. Microwave energy is fed to the cavity via waveguide 118, and is coupled thereto through slot 119.

In accordance with an aspect of the invention, reflector 114 is approximately spherical in shape. This causes the light to be reflected by the reflector back into the bulb. The resultant light which is re-emitted from the bulb is stronger

in higher wavelengths than in the case where light is not reflected back into the bulb.

This was demonstrated by the experimental setup depicted in FIG. 13, wherein the light emitted by the lamp is fed through baffles 120 and 121, which have co-linear openings 122 and 124 respectively disposed therein. A diffuser 125 backed by monochromator 126 is located in line with the baffle openings so as to receive the light coming therethrough.

Spectral measurements were taken for the case where the inside of reflector 114 is blackened, so as to be non-reflective, and the case where the reflector is shiny. The bulb was 2 cm in inner diameter and was filled with 2 mg/cc of elemental sulfur and 60 torr of argon, and was excited at a power density of about 325 watts/cc.

The resultant spectrum for the case where the reflector is blackened is shown in FIG. 14, while the spectrum for the case where the reflector is shiny is shown in FIG. 15. The data is expressed in irradiance (power per wavelength interval per square centimeter). As can be seen, not only does the lamp with shiny reflector produce a more intense output, but there is a greater concentration of higher wavelengths. This is shown more exactly in FIG. 16, which is a bar graph of the output power ratio of the lamp for shiny/black reflector. It is seen that the power ratio is about a factor of 2 in the yellow region of the spectrum, and a factor of about 3 in the red region. Thus, a lamp which is rich in such wavelengths may be produced by following the teachings of the invention.

Additionally, it was found that the output from the lamp with the shiny reflector was more uniform than that of the lamp with the black reflector, and while the bulb in the shiny reflector ran hotter than the bulb in the black reflector, it did not run much hotter, so that additional light power was obtained with only a modest increase in cooling requirement.

In accordance with a further aspect of the invention, selective wavelengths may be reflected back into the bulb to cause the lamp to emit a spectrum which is more equivalent to the spectrum radiated by a black body. For example, this may be effected with the use of dichroic reflectors in either discrete form, or disposed directly on the bulb in the form of a coating.

For example, if a dichroic reflector in the form of an optically thin filter which reflects only in the green region is disposed on the bulb, the output in the green region of the spectrum may be substantially cut, for example by a factor of 2. At the same time, the output in the red region of the spectrum increases.

Thus, a lamp having a spectrum produced by a sulfur fill modified as described above will emit more nearly like a black body. This is shown in FIG. 17, which is a 1931 chromaticity diagram. The position of the unfiltered output of such a lamp is shown at point D, where $x=0.320$ and $y=0.371$, while the position of the filtered output using a dichroic reflector which reflects only in the green region is shown at point E, which is at the black body line, where $x=0.341$ and $y=0.346$.

FIG. 18 shows an embodiment of the invention using a dichroic reflector/filter such as described above. In this embodiment, the dichroic reflector 130 is disposed on spherical bulb 92 which is located in reflector 134 which is closed by mesh 136. As known to those skilled in the art, such a dichroic reflector may be comprised of alternating layers of materials having different indices of refraction. For example, for reflecting in the green or green-yellow part of

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the spectrum around 540 nm with about a 50 nm bandwidth, a dichroic reflector comprised of 5 sets of alternating layers of zirconium oxide and silicon dioxide using layers 67.5 and 89 nm thick, respectively, may be used. As is known, the thickness and number of layers may be varied to change the spectral band which is reflected.

In accordance with a further aspect of the invention, the spectral output of the lamp may be tailored for particular applications by reflecting back selected wavelengths into the bulb. For example, a lamp in which green radiation is reflected back may be used for horticultural applications such as for plant growth as in greenhouses. Thus, the spectrum of the sulfur-based lamp is inherently high in green wavelengths, and these are attenuated by the dichroic filter, while the red wavelengths, which are useful in inducing plant growth are increased. Wavelengths other than green may be reflected back to produce different resultant spectral outputs.

It should be understood that while the invention has been illustrated in connection with specific embodiments, variations will occur to those skilled in the art, and the scope of the invention is to be limited only by the claims which are appended hereto and equivalents.

We claim:

1. A discharge lamp comprising,
 - a bulb comprised of an envelope and a fill in the envelope which includes sulfur when excited,
 - a source of excitation power,
 - means for coupling sufficient excitation power from said source to said fill to cause said sulfur to emit radiation which is principally in the visible part of the spectrum and is in the form of molecular radiation, and
 - reflector means for reflecting radiation which is emitted by the fill back into the fill, while allowing some radiation to exit the lamp, causing the radiation which exits the lamp to have proportionately more spectral power in the red region of the spectrum than if said radiation were not reflected back into the fill.
2. The lamp of claim 1 wherein said reflector means comprises means for reflecting a preponderance of the radiation which is emitted by the fill back into the fill.
3. The lamp of claim 2 wherein said bulb is electrodeless, and wherein both said bulb envelope and said reflector means are spherical in shape.
4. The lamp of claim 3 wherein said reflector means is separated from said bulb envelope.
5. The lamp of claim 3 wherein said reflector means is disposed on said bulb envelope.
6. The lamp of claim 3 wherein said reflector means preferentially reflects wavelengths in the green range, so as to cause the spectral output of the lamp to be closer or equivalent to that of a black body.

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7. The lamp of claim 6 wherein said reflector means comprises a dichroic reflector.

8. The lamp of claim 1 wherein the visible radiation which is emitted by said fill is primarily from said sulfur.

9. A discharge lamp comprising,

- a bulb comprised of an envelope and a fill in the envelope which includes selenium when excited,

- a source of excitation power,

- means for coupling sufficient excitation power from said source to said fill to cause said selenium to emit radiation which is principally in the visible part of the spectrum and is in the form of molecular radiation, and

- reflector means for reflecting radiation which is emitted by the fill back into the fill, while allowing some radiation to exit the lamp, causing the radiation which exits the lamp to have proportionately more spectral power in the red region of the spectrum than if said radiation were not reflected back into the fill.

10. The lamp of claim 9 wherein said reflector means comprises means for reflecting a preponderance of the radiation which is emitted by the fill back into the fill.

11. The lamp of claim 10 wherein said bulb is electrodeless, and wherein both said bulb envelope and said reflector means are spherical in shape.

12. The lamp of claim 11 where in said reflector means is separated from said bulb envelope.

13. The lamp of claim 11 wherein said reflector means is disposed on said bulb envelope.

14. The lamp of claim 11 wherein said reflector means preferentially reflects wavelengths in the green range, so as to cause the spectral output of the lamp to be closer or equivalent to that of a black body.

15. The lamp of claim 14 wherein said reflector means comprises a dichroic reflector.

16. A method of providing radiation, comprising the steps of,

- providing a lamp fill which upon excitation, contains at least one substance selected from the group of sulfur and selenium,

- exciting said lamp fill to cause said sulfur or selenium to produce a first spectral power distribution of primarily molecular radiation, and

- reflecting said produced radiation back into said fill to cause said fill to emit molecular radiation having a second spectral power distribution, which has a proportionately substantially greater amount of spectral power in the red region of the spectrum than said first spectral power distribution.

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United States Patent [19]
Simpson

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[45] **Date of Patent:** **Feb. 29, 2000**

[54] **COMPACT MICROWAVE LAMP HAVING A TUNING BLOCK AND A DIELECTRIC LOCATED IN A LAMP CAVITY**

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[52] **U.S. Cl.** 315/39; 315/248

[58] **Field of Search** 315/39, 248, 267, 315/344

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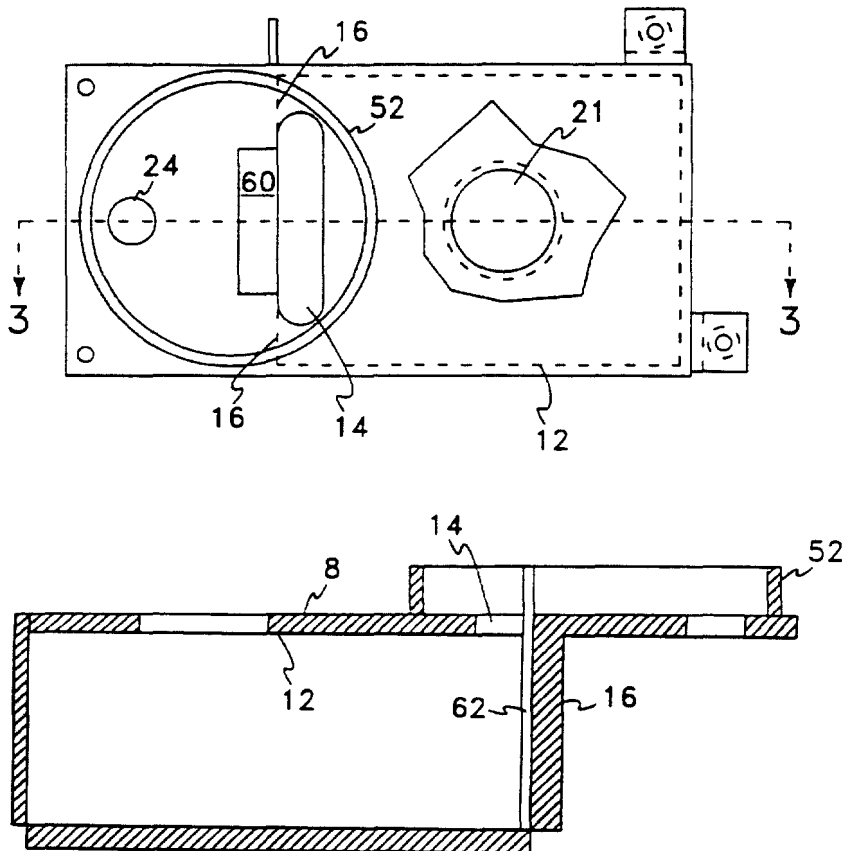
0 153 745	9/1985	European Pat. Off.	H01J 65/04
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93/21655	10/1993	WIPO	H01J 16/38

Primary Examiner—Benny T. Lee

[57] **ABSTRACT**

A microwave lamp having a compact structure utilizing a coupling slot which has a dielectric member extending therethrough and a tuning block adjoining the coupling slot. A non-conventional waveguide is used which has about the width of a WR-284 waveguide and about the length of a WR-340 waveguide.

10 Claims, 3 Drawing Sheets



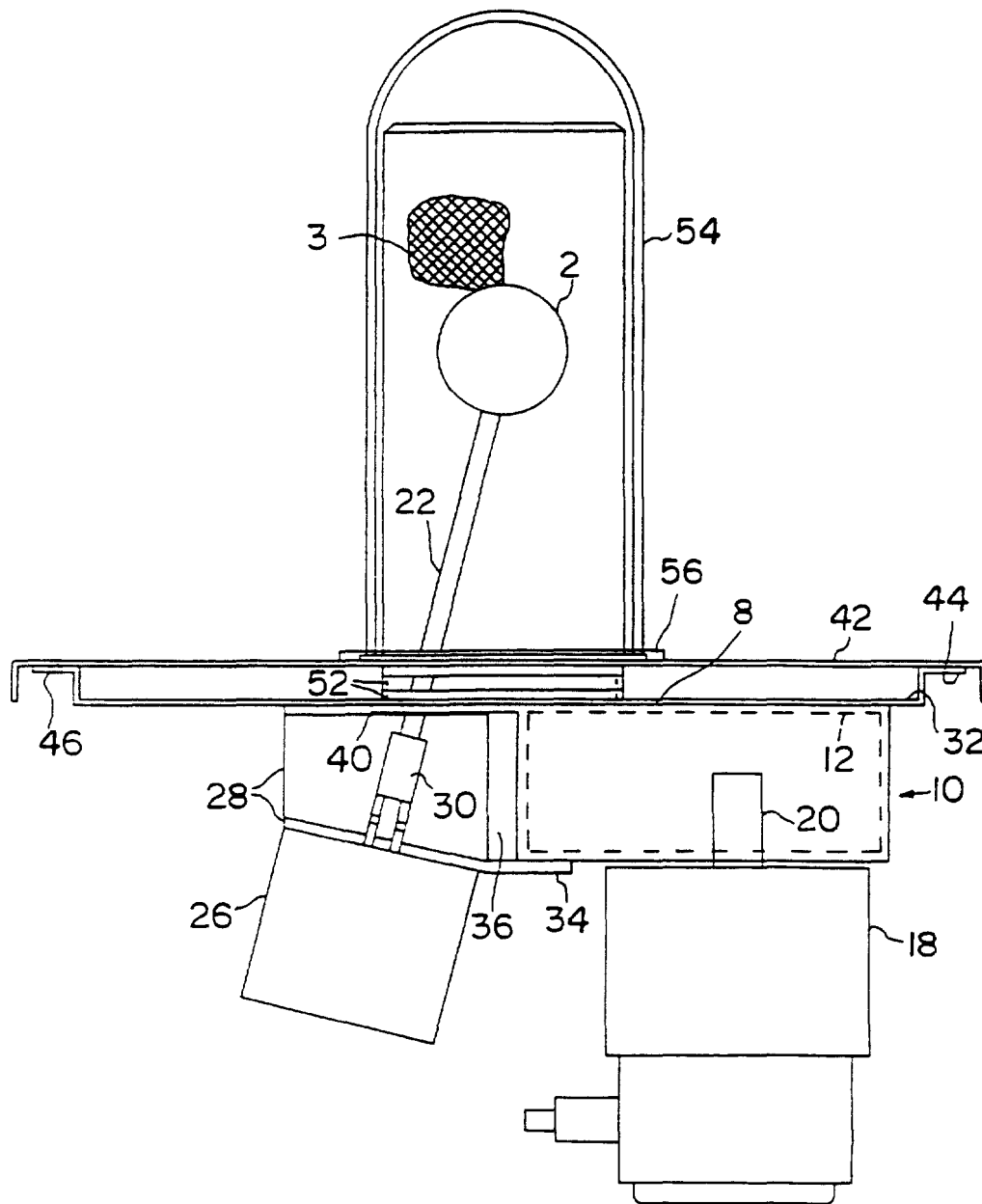


FIG. 1

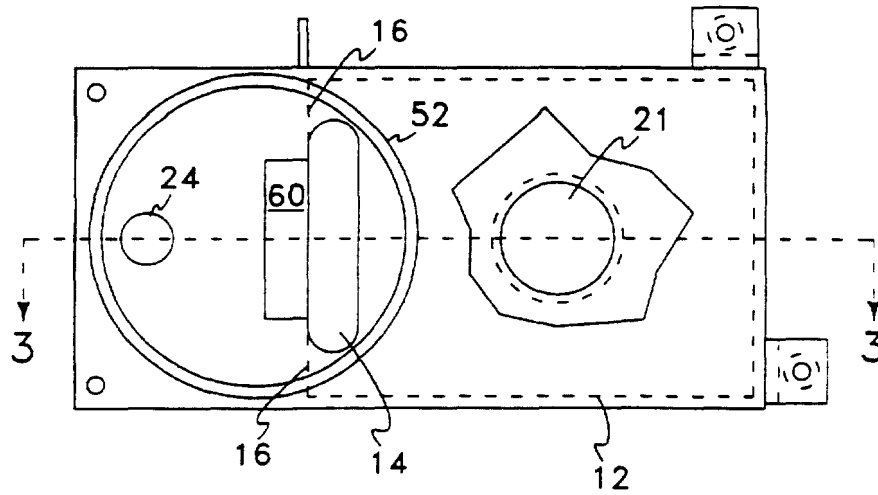


FIG. 2

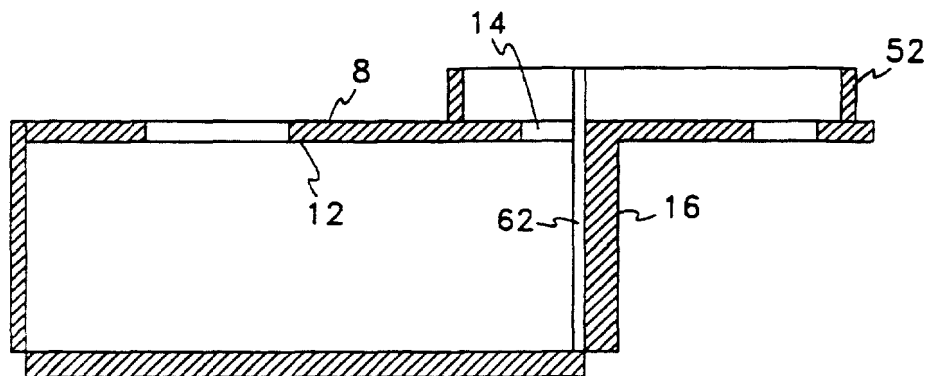


FIG. 3

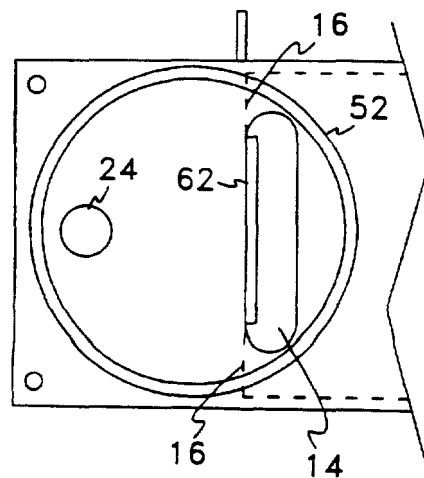


FIG. 3A

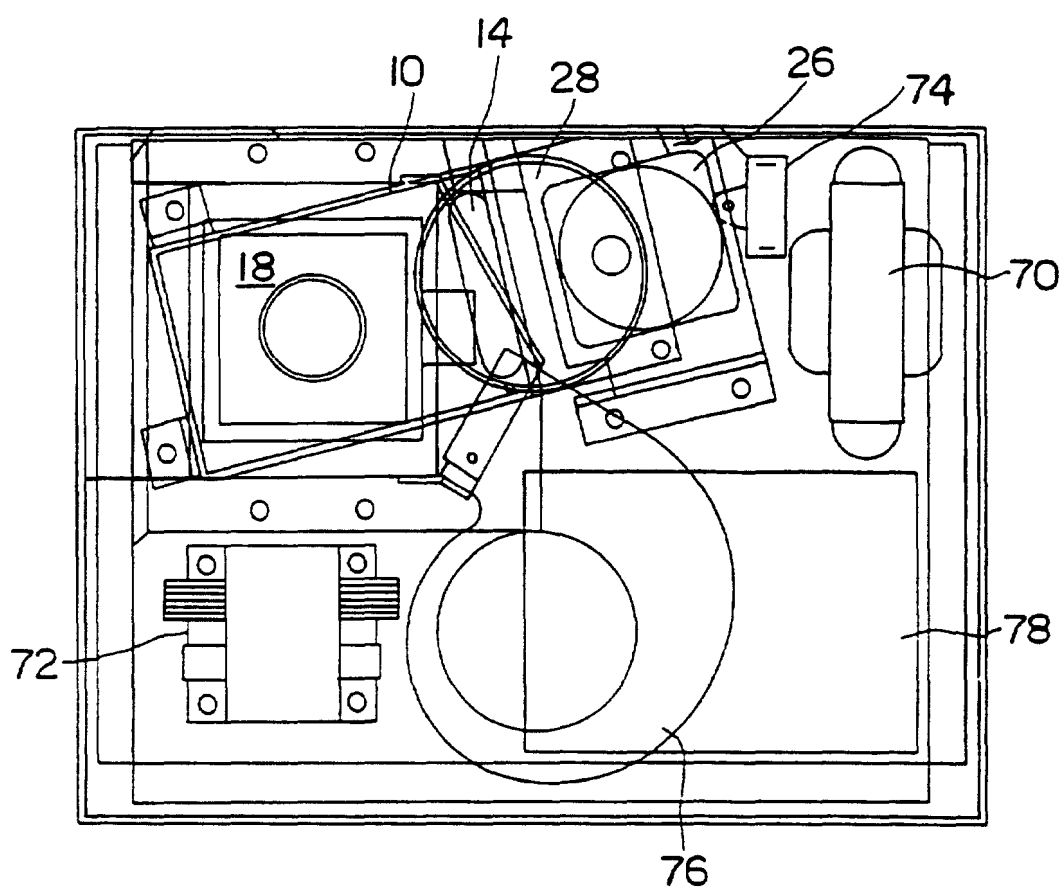


FIG. 4

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COMPACT MICROWAVE LAMP HAVING A TUNING BLOCK AND A DIELECTRIC LOCATED IN A LAMP CAVITY

This application has been filed under 35 U.S.C 371 based on PCT Application No. PCT/US96/05556, filed Apr. 22, 1996, which has priority based on U.S. patent application Ser. No. 426,603, filed Apr. 21, 1994, now abandoned.

The United States Government has certain rights to the subject matter described herein under an award from the Department of Energy.

BACKGROUND OF THE INVENTION

The present invention relates to a microwave powered lamp, and particularly to such a lamp which has a compact structure.

Recently, microwave powered lamps utilizing sulfur or selenium based fills for efficiently radiating in the visible region have been disclosed. For example, see U.S. Pat. No. 5,404,076, issued Apr. 4, 1995, which is incorporated herein by reference.

Such microwave lamps may be used as illumination sources, which find a particular use in commercial or industrial lighting. For such lighting applications, it is desirable to build a lamp system which fits within the general outline of some of the lamps already in existence. Many of these are equipped with rather large inductive ballasts which are installed in overhead locations adjoining the associated lamp. Accordingly, a new lamp system will have greater utility if it occupies a package of comparable size which can be similarly placed. This requires the various parts of the electrodeless lamp system to be kept as small as reasonably possible. These parts include a quartz bulb to contain the arc plasma housed within a microwave cavity having a metal mesh to contain the microwaves but allow the escape of light, a magnetron to produce the microwaves, a waveguide to carry the microwaves from the magnetron to the cavity, a power supply to drive the magnetron and cooling fans or other means to cool the magnetron and its power supply. The lamp bulb is rotated within the microwave cavity to stabilize the discharge which adds a motor to the system as well.

To increase the versatility of the new lamp and, therefore, the number of sites in which it can be used, the lamp itself does not include a reflector. Rather the lamp is to be inserted through a hole in reflectors of several designs, suitable for use in applications requiring light dispersal over different areas. This requires the light source to extend outward from the lamp case a distance of at least 100 mm. Keeping the entry hole to a small diameter increases the efficiency of the reflector.

It is desirable to keep the overall length of the lamp as small as possible. Since the motor which rotates the bulb must be placed outside of microwave fields, it potentially adds length to the lamp system. In one such configuration, the bulb stem is fed through the coupling slot and the waveguide, and the motor and coupler are located on the other side of the waveguide, resulting in a very long stem which is subject to breakage.

A further problem is encountered in that the waveguide must have a sufficiently narrow width so that the cutoff frequency is high enough to eliminate spurious interference signals from being generated, but must have a height sufficient to prevent arcing at the location of the magnetron antenna. A conventional WR-284 waveguide is narrow enough to eliminate interference signals, but because of its height which correlates to its width in a conventional ratio of about 1 to 2, arcing results.

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SUMMARY OF THE INVENTION

It is thus an object of the invention to provide a microwave powered illumination lamp having a compact structure.

It is a further object of the invention to provide a microwave powered illumination lamp wherein the stem supporting the bulb is not very long.

It is still a further object of the invention to provide a lamp in which arcing is obviated.

In accordance with a first aspect of the invention, a microwave lamp is provided wherein the coupling slot is located in the cavity end wall to one side of center, while the bulb stem passes through the end plate to the other side of center and is at an angle of other than 90° in relation to the end wall, so that the bulb is supported centrally in relation to the cavity wall structure. A motor and shaft coupling to the bulb stem are located at the end of the stem outside the cavity. In this manner, the bulb stem which is provided is not particularly long, and therefore provides a more rugged and durable support structure.

In accordance with a further aspect of the invention, the waveguide which feeds the coupling slot is oriented so that its longitudinal dimension is parallel to the cavity end wall, thus minimizing the overall length of the lamp.

In accordance with a still further aspect of the invention, a novel waveguide structure is used, wherein the waveguide has about the height of a WR-340 waveguide, while it has the width of a WR-284 waveguide. In this way, the height of the magnetron antenna is accommodated without arcing, while spurious signals which might cause interference are eliminated.

BRIEF DESCRIPTION OF THE DRAWINGS

The invention will be better understood by referring to the accompanying drawings, wherein:

FIG. 1 is a side view of a lamp in accordance with an embodiment of the invention.

FIG. 2 is a top view of the waveguide portion of the lamp depicted in FIG. 1.

FIG. 3 is a sectional view of the waveguide of the lamp of FIG. 1 taken perpendicular to the coupling slot along section line 3—3 in FIG. 2.

FIG. 3A is a top, fragmented view of the waveguide showing a dielectric member substantially as wide as the coupling slot.

FIG. 4 is a plan view which depicts how the magnetron and associated components are mounted in the lamp of FIG. 1.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Referring to FIG. 1, a lamp in accordance with an embodiment of the invention is shown. The lamp is comprised of bulb 2 which is located in a microwave cavity. The bulb may be made of quartz and encloses a discharge forming medium, for example, a sulfur or selenium based fill.

The microwave cavity is cylindrical, and is comprised of a side wall structure, and two end walls. The side wall structure and top end wall in the orientation of FIG. 1 are made of a cylindrical metallic mesh, shown in part at reference numeral 3, which allows light to exit but is substantially opaque to microwave radiation. The bottom end wall of the cavity in the orientation of FIG. 1 is the outside surface 8 of waveguide 10.

As mentioned above, the microwave lamp depicted in FIG. 1 may be used to replace existing non-microwave lamps, and it is therefore desirable for the lamp to be made as compact as possible so as to fit within the general outline of existing lamps.

In some microwave lamps of the prior art wherein the bulb stem extends from an end wall, it passes through the waveguide which feeds the cavity, and the motor and coupling ferrule are mounted on the opposite side of the waveguide, far enough away to be clear of microwave fields. Such an arrangement, however, may have the effect of increasing the overall length of the lamp, as well as the length of the bulb stem, thereby making it subject to breakage.

In accordance with the present invention, the coupling slot is located to one side of center in the cavity end wall, while the bulb stem is fed through the end wall to the other side of center canted in relation to the end wall, with the motor and ferrule being mounted outside the cavity and away from the waveguide. Additionally, the longitudinal direction of the waveguide extends parallel to the end wall of the cavity, so as to not extend the length of the lamp. The result is a more compact lamp of shorter overall length, wherein the bulb is more ruggedly supported on a shorter stem.

Referring to FIGS. 1 and 2, rectangular waveguide 10 is shown, having inside wall 12 and outside wall 8 (see FIG. 1). The top walls of the waveguide have coupling slot 14 therein, which is shown in FIG. 2. As is also shown in FIG. 2, end wall 16 of the waveguide is slightly wider than the coupling slot 14.

Returning to FIG. 1, magnetron 18 having antenna 20 is mounted to the waveguide, as shown. Microwave power is fed into the waveguide and through coupling slot 14 (see FIG. 2) to the microwave cavity, where it excites the fill in bulb 2. In FIG. 2, hole 21 is shown, through which the magnetron antenna and a gasket protrude.

Referring to FIG. 1, bulb stem 22 is passed through hole 24 at (see FIG. 2) an angle of other than 90°, (about 77° in the preferred embodiment) so that the bulb is centrally located in relation to the mesh side wall structure of the cavity. The motor 26 is mounted to motor support 28, while ferrule 30 couples the motor shaft to the bulb stem, which is typically made of quartz. Extension 34 of support 28 is secured to the bottom outside surface of the waveguide, while gap 36 is present between the motor support and the end wall of the waveguide.

In FIG. 1, the top wall 8 of the waveguide extends to the left at reference numeral 40 past the end of the waveguide. Additionally, the top of the waveguide is flush against plate 32, which is secured to plate 42 at the ends thereof with flanges 44 and 46. Referring to FIGS. 1 and 2, metallic ring 52 is mounted on the top surface of the waveguide (cavity end). The cylindrical mesh is secured to this ring by a clamp, and the mesh passes through a hole in plate 42. As shown in FIG. 1a cylindrical envelope 54 which may be made of glass or quartz surrounds the screen, and is mounted on plate 42, for example by retainer 56. Thermal insulation is disposed in the space between plates 32 and 42.

In the operation of the lamp, microwave power generated by the magnetron is fed through the waveguide and the coupling slot into the cavity in which bulb 2 is located. In order to make the device as compact as possible and to provide a stable relationship between the magnetron and the cavity, magnetron antenna 20 is located $\frac{1}{4}$ guide wavelength (the wavelength of signals propagating within the waveguide) from coupling slot 14.

Additionally, it was found that a waveguide having a width sufficiently narrow to have a cut-off frequency sufficiently high to eliminate spurious signals was necessary. For example, a waveguide was tried which accommodated the magnetron antenna produced out of band signals 200 Mhz below the normal operation point of 2450 Mhz, and the use of the $\frac{1}{4}$ wavelength waveguide length referred to above tends to aggravate this situation. It was found that a WR-284 (equivalent IEC designation, R-32) waveguide was sufficiently narrow to eliminate spurious signals, but it was found that the height of this waveguide was too small to accommodate the magnetron antenna without arcing. To solve this problem, a non-conventional waveguide was used having about the width of the WR-284 waveguide and about the height of the WR-340 (equivalent IEC designation, R-26) waveguide. This blocks the transmission of signals below 2078 Mhz and helps to suppress the low frequency out of band signals by reducing the phase shift between the magnetron and the coupling slot. At the same time, the height of the waveguide is sufficient to accommodate the magnetron antenna without arcing.

The waveguide end wall behind the magnetron is moved farther away than is the usual practice. In prototype testing, a metal tuning knob was used to match the impedance of the lamp to the waveguide. This knob functioned as a capacitor at its location. With the length reduction to one quarter wavelength, this position became the same as the magnetron antenna. A tuning knob might have been placed beside the antenna, taking care to avoid arcing, however, the magnetron antenna itself is a capacitor across the waveguide. This is usually compensated by placing the end wall in an inductive position, closer to the antenna than a quarter wavelength. By moving the wall farther out, the inductance is reduced and the antenna is seen as the desired tuning capacitance. The best position was found experimentally by using a movable waveguide end wall.

In many previous microwave lamps, matching is accomplished by placing a tuning knob in the waveguide. If all possible load phases are to be corrected, a half-wavelength of waveguide is needed. According to the invention, the system was matched by placing a thin tuning block 60 inside the microwave cavity, shown in FIG. 2, beside the slot 14 to modify the current path. For example, block 60 may comprise a fixed metallic tuning member adjacent to the slot 14.

Referring to FIG. 3, which is a view as seen from the back of the lamp in FIG. 1 (left to right reversed), dielectric member 62, which may be made of mica is depicted. This member is secured, for example, against the inside end wall 16 of the waveguide and protrudes through coupling slot 14 while contracting the edge of the slot. It may be substantially as wide as the slot (see FIG. 3A). The purpose of member 62 is to prevent arcing across the slot. Elements 8, 12, and 52 reference like numbered elements previously described.

FIG. 4 is a plan view of the magnetron and associated components, which are located on plate 32 shown in FIG. 1.

As seen in FIG. 4, the magnetron 18 receives filament power from filament transformer 70, while stepdown transformer 72 may be used to provide power for bulb rotator motor 26, shown in connection with motor mount 28 and capacitor 74. In FIG. 4, magnetron cooling air blower 76 is depicted as is PC control board 78. Finally, waveguide 10 is shown feeding coupling slot 14.

While the invention has been described in connection with a preferred embodiment, variations will occur to those skilled in the art, and it is therefore understood that the invention herein is defined in the claims which are appended hereto.

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I claim:

1. An electrodeless lamp, comprising:
 - a microwave cavity having a light-transmissive portion;
 - a bulb disposed in the microwave cavity, the bulb containing a discharge forming fill;
 - a source of microwave power;
 - a waveguide coupled to the source of microwave power, the waveguide including a slot in a wall of the waveguide for coupling the microwave power to the microwave cavity; and
 - a tuning block positioned inside the microwave cavity adjoining the slot.
2. The electrodeless lamp as recited in claim 1, wherein the tuning block comprises a fixed metallic tuning member.
3. An electrodeless lamp, comprising:
 - a microwave cavity having a light-transmissive portion;
 - a bulb disposed in the microwave cavity, the bulb containing a discharge forming fill;
 - a source of microwave power;
 - a waveguide coupled to the source of microwave power, the waveguide including a slot in a wall of the waveguide for coupling the microwave power to the microwave cavity; and
 - a dielectric member positioned against an end wall of the waveguide and extending into the microwave cavity along an edge of the slot.
4. The electrodeless lamp as recited in claim 3, wherein the end wall of the waveguide is substantially aligned with the edge of the slot, and wherein the dielectric member extends through the slot and is secured to the end wall of the waveguide.
5. The electrodeless lamp as recited in claim 3, wherein the dielectric member is comprised of mica.

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6. The electrodeless lamp as recited in claim 3, wherein the dielectric member has a width which is substantially as wide as a width of the slot.

7. A compact electrodeless lamp, comprising:

- a microwave cavity having a light-transmissive portion;
- a bulb disposed in the microwave cavity, the bulb containing a discharge forming fill;
- a magnetron for providing microwave power, the magnetron having an antenna;
- a waveguide connected to the magnetron so that the antenna of the magnetron extends inside the waveguide, the waveguide including a slot in a wall of the waveguide for coupling the microwave power to the microwave cavity,

wherein the distance between the antenna and the slot is about $\frac{1}{4}$ guide wavelength,

and wherein the waveguide has a width which is sufficiently narrow to suppress out of band signals and a height sufficient to avoid arcing between the waveguide and the antenna.

8. The electrodeless lamp as recited in claim 7, further comprising a dielectric member positioned against an end wall of the waveguide and extending into the microwave cavity along an edge of the slot.

9. The electrodeless lamp as recited in claim 7, further comprising a tuning block positioned inside the microwave cavity adjacent to the slot.

10. The electrodeless lamp as recited in claim 7, wherein the width of the waveguide is about equal to a width of a WR-284 waveguide and wherein the height of the waveguide is about equal to a height of a WR-340 waveguide.

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